Break it, or Lose it: Thermal Bridging in Building Envelopes

NESEA BuildingEnergy 16

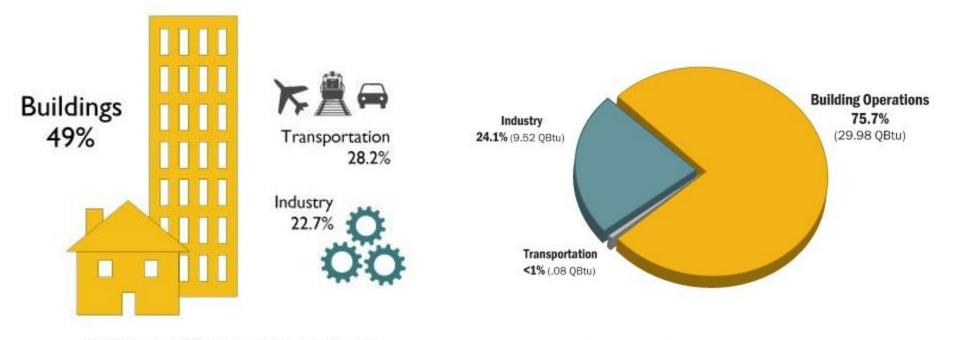
March 9, 2016



INTRODUCTION | Learning Objectives

- 1. Learn the significance that thermal bridges can have on decreasing the design intended R-value in commercial building facades.
- 2. Will know common problems areas in the thermal performance of building envelopes which can be used to identify potential problems in future designs.
- 3. Learn a methodology for evaluating thermal bridges through thermal imaging that can be used to evaluate building during and after construction.
- 4. Will learn the limitations of current processes for evaluating heat flows through building envelopes and an easily applied simulation technique to correctly evaluate it.

INTRODUCTION | Building's Environmental Impact



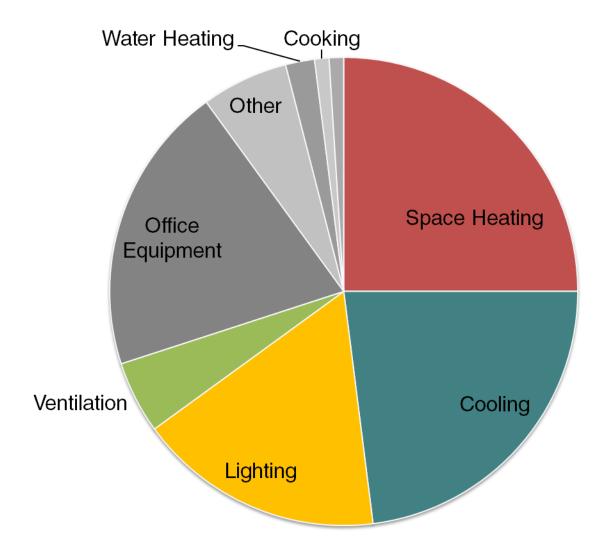
U.S. Energy Consumption by Sector

Source: @2010 2030. Inc. / Architecture 2030. All Rights Reserved. Data Source: U.S. Energy Information Administration (2009).

U.S. Electricity Consumption by Sector

Source: @2011 2030, Inc. / Architecture 2030. All Rights Reserved. Data Source: U.S. Energy Information Administration (2011).

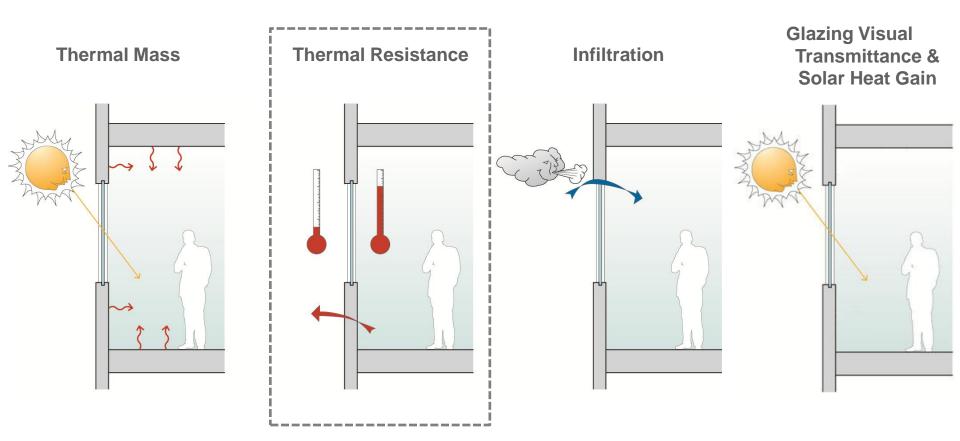
INTRODUCTION | Architect's Influence on Energy Usage



70%

of commercial building's energy is impacted by the design of the envelope

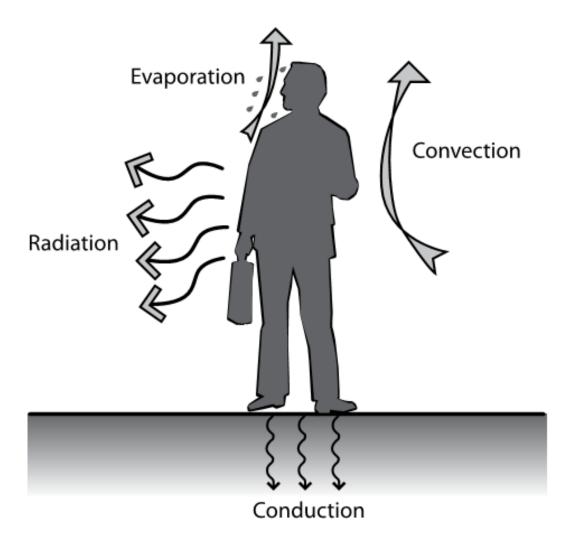
INTRODUCTION | Envelope's Impact on Energy



INTRODUCTION | Heat Flow Basics

Modes of Heat Transfer:

- Conduction
- Convection
- Radiation



INTRODUCTION | Heat Flow Basics

Heat flow through the building envelope (Q)

 $Q = A \times U \times \Delta T$ (in Btu/hr or W)

 $\Delta T = area of surface$ $\Delta T = difference in temperature between inside & out$ U = heat transfer coefficient INTRODUCTION | Heat Flow Basics

 R-value – measure of thermal resistance - h·ft^{2.°}F/Btu or m^{2.°}K/W

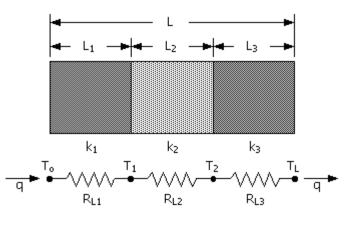
(bigger the better)

 U-value – heat transfer coefficient; measure of how well the building conducts heat - Btu/h-ft²·°F or W/m²·°K (smaller the better)

 $U = \frac{1}{R} = \frac{material \ conduct}{material \ width} = \frac{heat \ transfer \ per \ unit \ area}{temperature \ difference}$

INTRODUCTION | Thermal Bridges

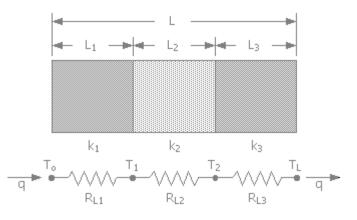
How we think about it in design:



1D Heat Flow

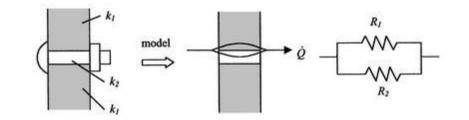
INTRODUCTION | Thermal Bridges

How we think about it in design:



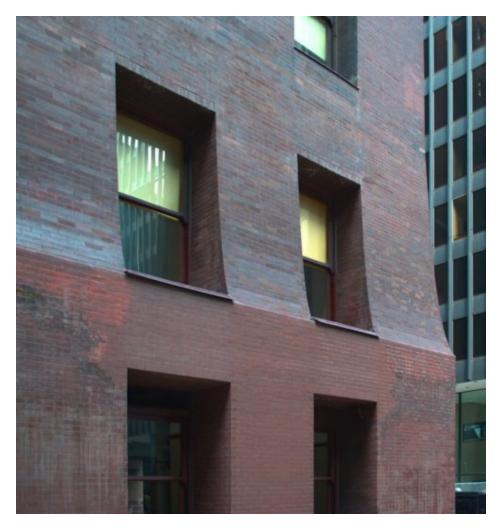
1D Heat Flow

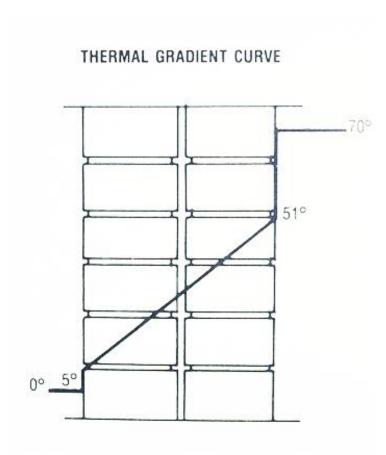
How it is in reality:



2D & 3D Heat Flow

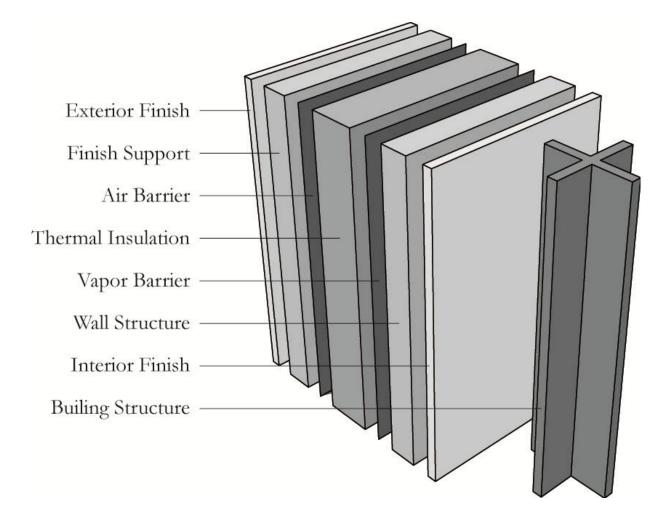
INTRODUCTION | Historic Envelopes



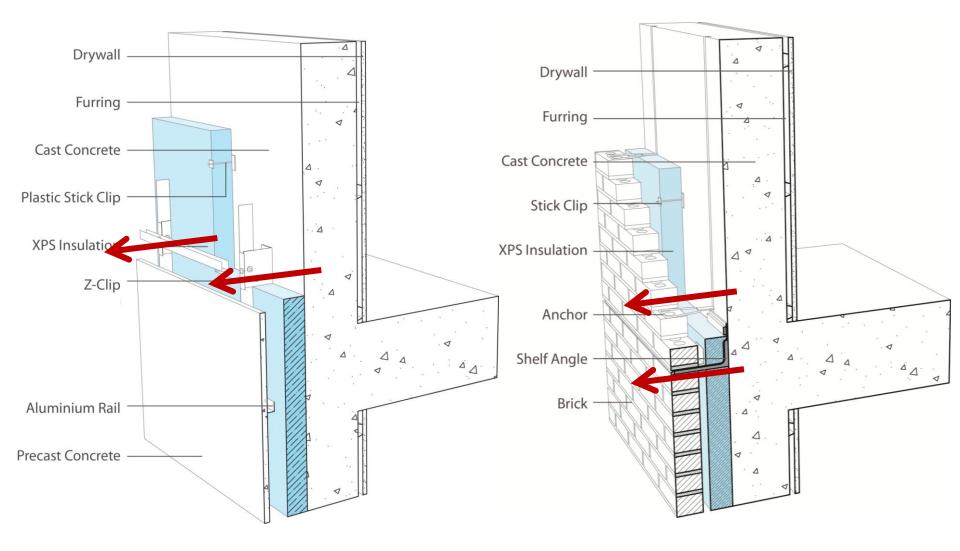


Monadnock Building in Chicago, IL

INTRODUCTION | Modern Envelopes



INTRODUCTION | Modern Envelopes



INTRODUCTION | Code Requirements

• Specify Minimum R-values

From ASHRAE 90.1-2007

 TABLE 5.5-5
 Building Envelope Requirements For Climate Zone 5 (A, B, C)*

Opaque Elements	Nonresidential		Residential		Semiheated	
	Assembly Maximum	Insulation Min. R-Value	Assembly Maximum	Insulation Min. R-Value	Assembly Maximum	Insulation Min. R -Value
Roofs						
Insulation Entirely above Deck	U-0.048	R-20.0 c.i.	U-0.048	R-20.0 c.i.	U -0 .119	R-7.6 c.i.
Metal Building	U-0.065	R-19.0	U-0.065	R-19.0	U-0.097	R-10.0
Attic and Other	U-0.027	R-38.0	U-0.027	R-38.0	U-0.053	R-19.0
Walls, Above-Grade						
Mass	U-0.090	R-11.4 c.i.	U-0.080	R-13.3 c.i.	U-0.151 ^a	R-5.7 c.i. ^a
Metal Building	U-0.113	R-13.0	U-0.057	R-13.0 + R-13.0	U-0.123	R-11.0
Steel-Framed	U-0.064	R-13.0 + R-7.5 c.i.	U-0.064	R-13.0 + R-7.5 c.i.	U-0.124	R-13.0
Wood-Framed and Other	U-0.064	R-13.0 + R-3.8 c.i.	U-0.051	R-13.0 + R-7.5 c.i.	U-0.089	R-13.0
Walls, Below-Grade						
Below-Grade Wall	C-0.119	R-7.5 c.i.	C-0.119	R-7.5 c.i.	C-1.140	NR
Floors						
Mass	U-0.074	R-10.4 c.i.	U-0.064	R-12.5 c.i.	U-0.137	R-4.2 c.i.
Steel-Joist	U-0.038	R-30.0	U-0.038	R-30.0	U-0.052	R-19.0
Wood-Framed and Other	U-0.033	R-30.0	U-0.033	R-30.0	U-0.051	R-19.0

INTRODUCTION | Code Requirements

 Continuous insulation – insulation that is continuous across all structural members without thermal bridges other than fasteners and service openings.

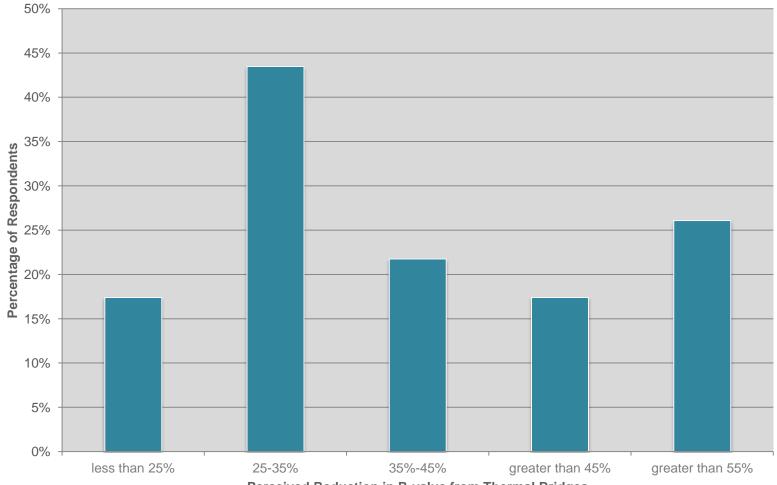
INTRODUCTION | Code Requirements

- Continuous insulation insulation that is continuous across all structural members without thermal bridges other than fasteners and service openings.
- Structural Members IE studs, Z-girts, clips
- Fasteners IE screws & nails

How many facades meet these requirements?

HYPOTHESIS | Survey

What is the impact on the R-value of thermal bridges in commercial assemblies?

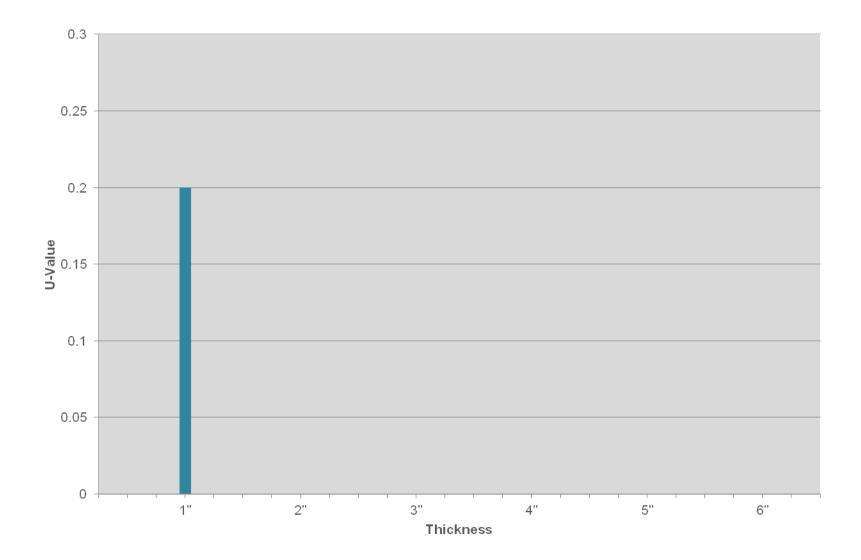


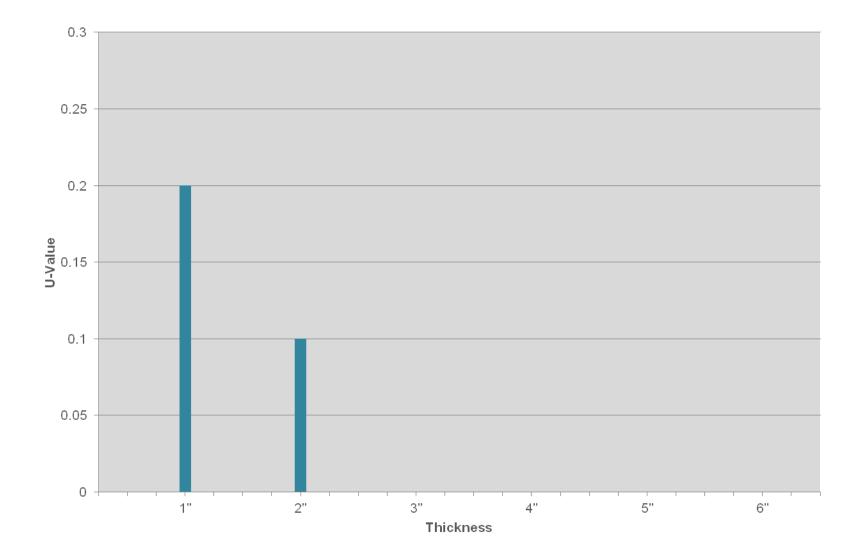
Perceived Reduction in R-value from Thermal Bridges

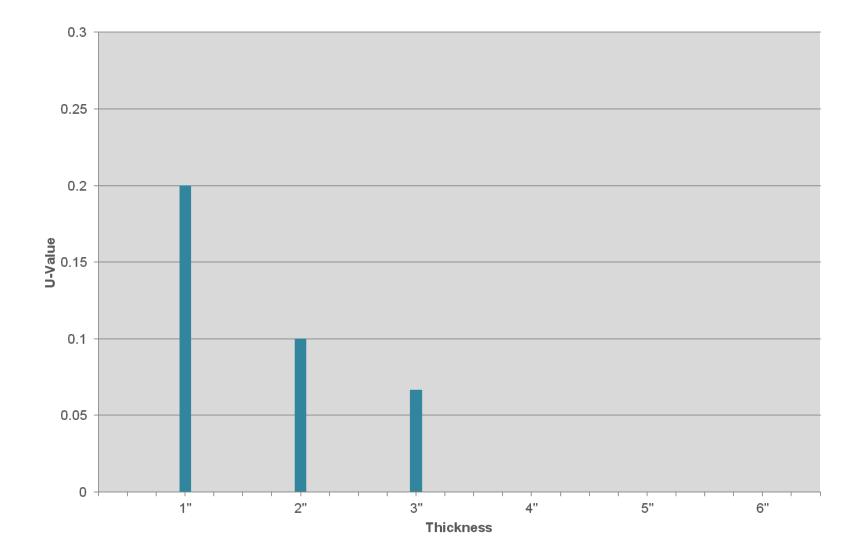
HYPOTHESIS | Existing Literature

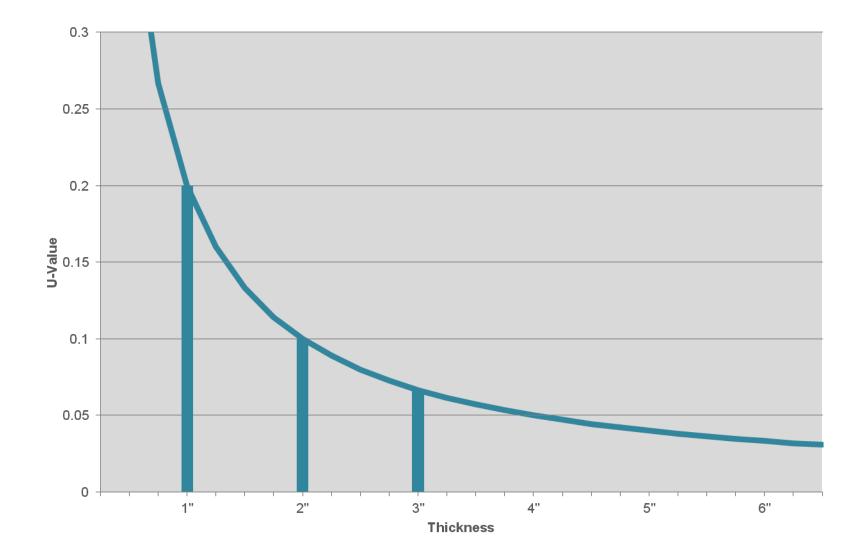
What is the impact on the R-value of thermal bridges in commercial assemblies?

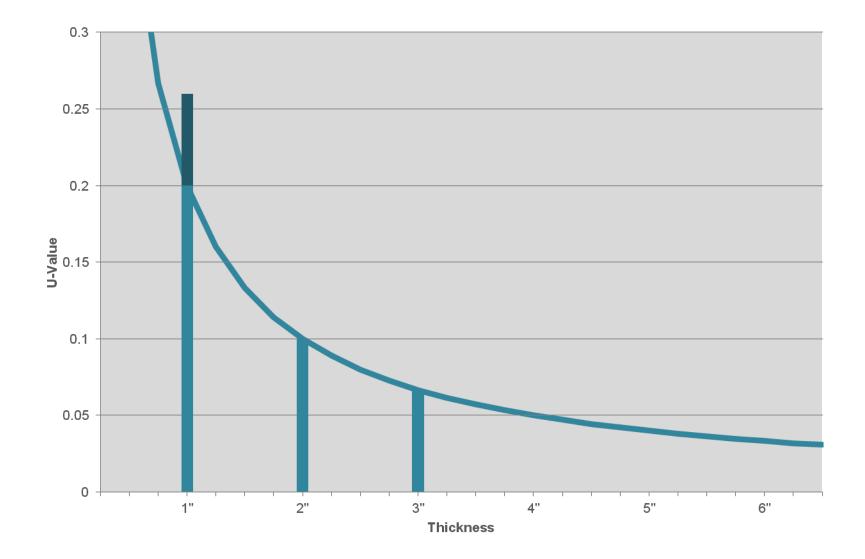
• Very little literature exists, but those that do suggest they can have a significant impact

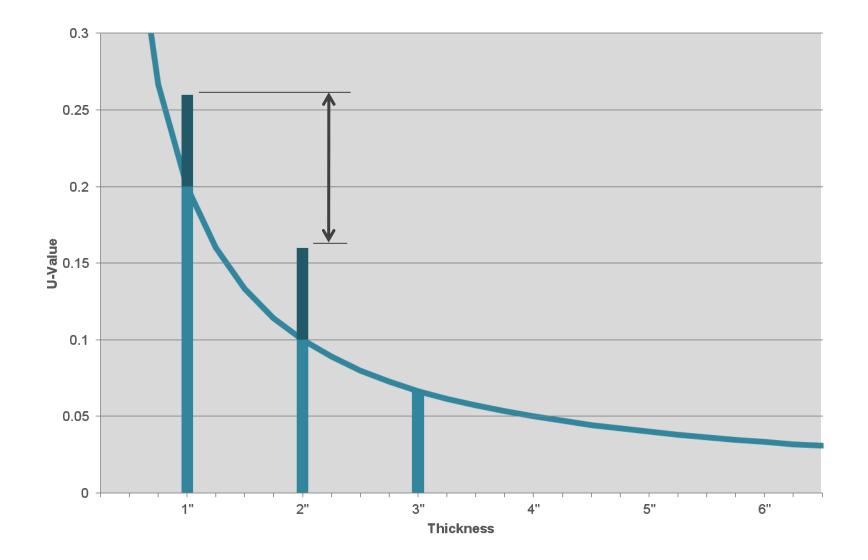


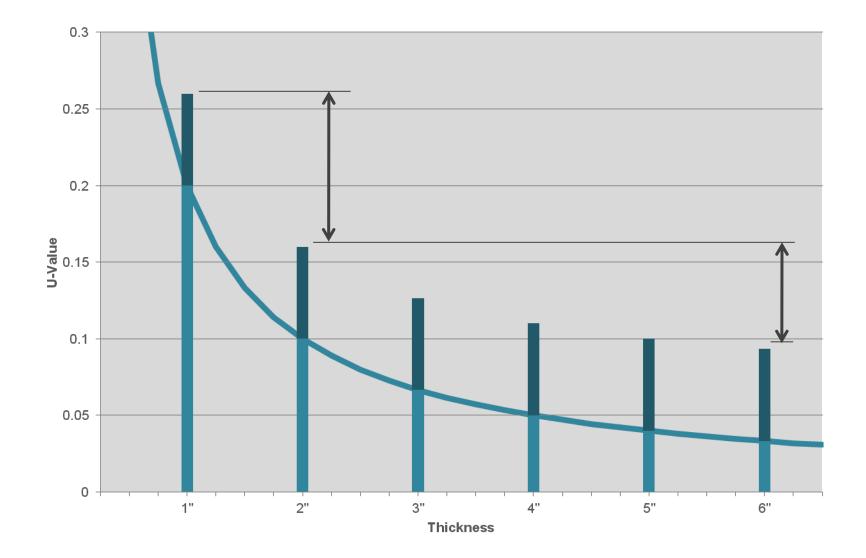


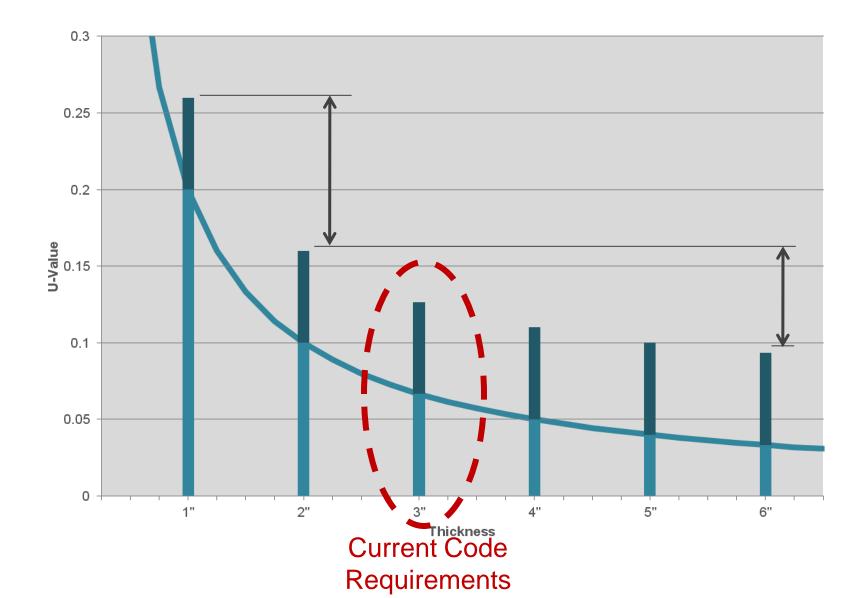




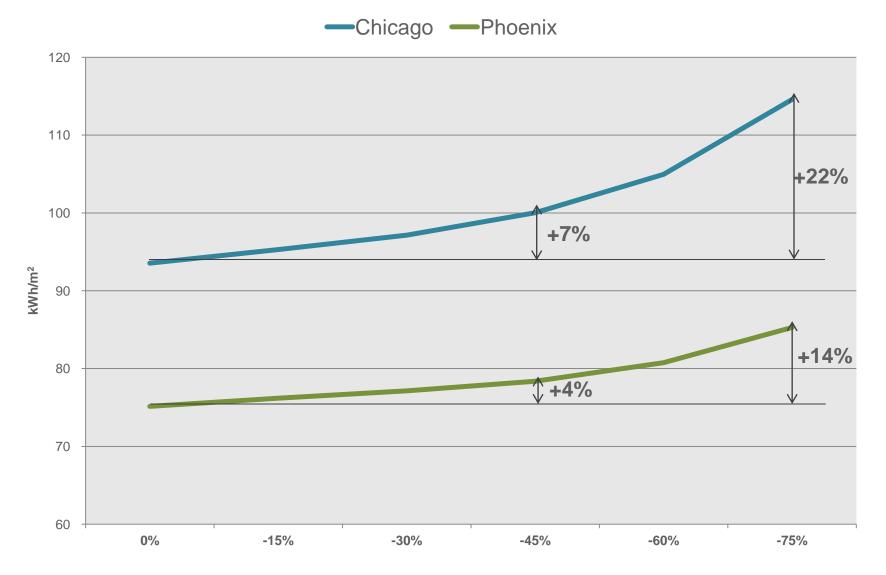








HYPOTHESIS | Decrease in R-value's Impact on Energy

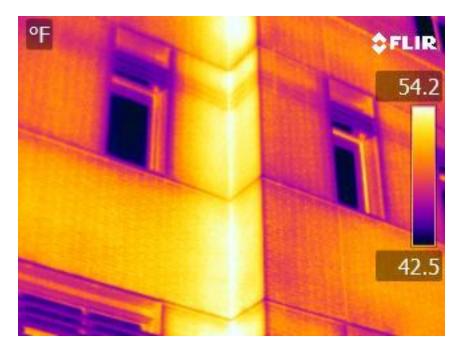


Energy Model Based on DOE Benchmark Model for Large Office Building Updated to High Performance Building (ASHRAE 90.1-2010)

HYPOTHESIS | Hypothesis

Thermal bridges have a big impact on the thermal performance of our facades. Changing how we design our envelope will have a biggest impact in improving their thermal performance.

- Quantify how walls are really performing and understand the impact of thermal bridges
- Identify if any observed decreases in thermal performance is resultant from design decisions or construction practices
- Identify good (and bad) design details for thermal performance

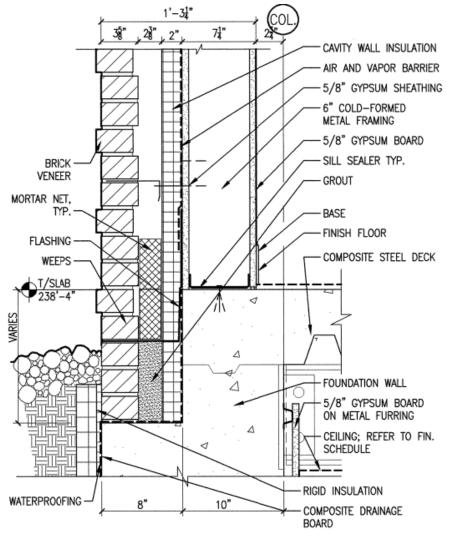


RESEARCH PROCESS | Baseline R-Value

 Manual calculation based on design - Doesn't account for thermal bridges and is viewed as "best case scenario"

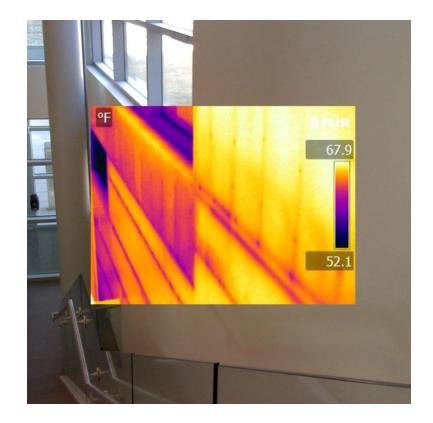
Material	Thickness	k	R-value	
Ext. Air	NA	-	0.17	
Brick	3.625	6.4	0.56	
Air Space	2.375	-	0.91	
XPS	2	0.2	10.00	
Gypsum	0.625	1.1	0.57	
Studs	6	-	1.36	
Gypsum	0.625	1.1	0.57	
Int. Air	NA	-	0.68	

R-value = 14.82



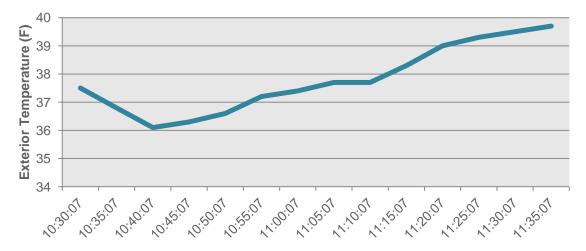
RESEARCH PROCESS | Observed Performance

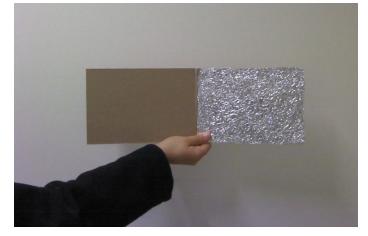
- Use thermal imaging camera to document actual performance in 15
 buildings
- Creates color infrared image of surface temperature



RESEARCH PROCESS | Observed Performance

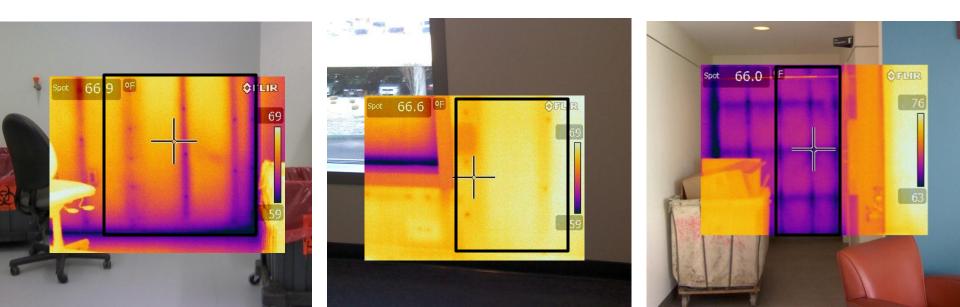
- Calculate R-value from thermal images
- Calculation based on difference between wall surface and inside air temperature, inside surface and radiant temperature, and inside surface and exterior temperature.
- Need to also find out:
 - Outside Air Temperature
 - Inside Air Temperature
 - Inside Radiant Temperature



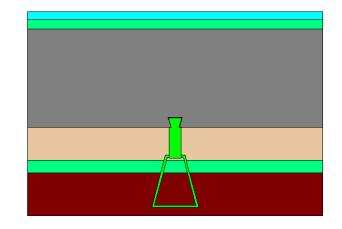


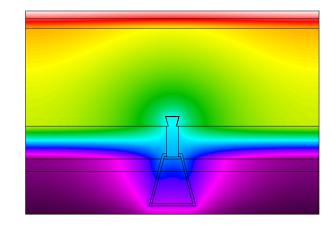
RESEARCH PROCESS | Limitation of Thermal Image

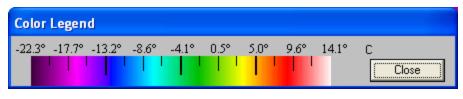
- R-value only of designated area
- Calculated only from interior
- Doesn't work on glass because it is a specular reflector
- Can only take images in winter (in the northeast) when there is a larger temperature difference between interior & exterior



- Use THERM 2D heat flow simulation program to match model with image to better understand what is causing decrease in R-value
- Validated model allows for testing of alternative designs
- Provides results of U-value along specified surface, surface temperatures and images of temperature gradient through model







How to make a 2D program simulate a 3D world:

Parallel Path Measured **Isothermal Planes** Averaged °C °C % Different °C % Different °C % Different Nylon, 229mm 12.4 11.5 -7.3% 11.5 -7.3% 11.5 -7.3% Stainless,457mm 11.0 10.5 -0.9% 11.3 +2.7% -4.5% 10.9 Stainless,305mm 10.8 11.2 +3.7%10.1 -6.5% 10.7 -0.9% Stainless,229mm 10.7 +3.7% 9.8 10.5 -1.9% 11.1 -8.4% Stainless,152mm 10.5 +3.8% 9.2 10.9 -12.4% 10.1 -3.8% Stainless, 76mm 9.4 10.3 +9.6% 7.9 9.1 -3.2% -16.0% Steel, 229mm 8.8 11.1 +26.1% 7.7 -12.5% 9.4 +6.8% $\pm 8.1\%$ -9.7% ± 3.5% Average

Table 22: Average Surface Temperature Results Comparision (Griffith 1997)

Parallel Path Method

- Weighted average of 2 simulations

 $U_{\text{P}} \equiv F_{\text{B}} \ast U_{\text{B}} + F_{\text{N}} \ast U_{\text{N}}$

Whereas, $U_P = U$ -value parallel path

 $F_B = Fraction of bridging element$

 $U_B = U$ -value from THERM with bridging element

 $F_N =$ Fraction of clear wall

 $U_N = U$ -value from THERM of clear wall

Isothermal Planes Method

- 1 simulation with a weighted average of the conductivities

 $k_{eff} = F_B * k_B + F_N * k_N$

Whereas, $U_I = U$ -value from THERM using isothermal planes method

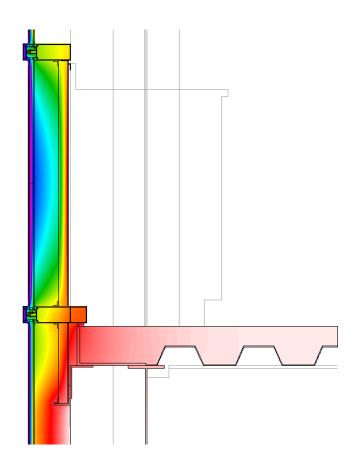
 $k_B = effective \ conductivity$

 k_{B} = conductivity of bridging element

 $k_N = conductivity of non-bridging element$

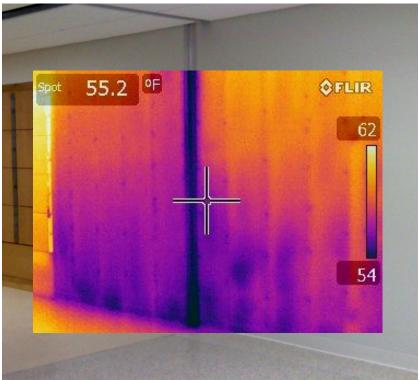
RESEARCH PROCESS | Identified Commonalities

- Identified 16 common areas for further investigation
- Cladding Support Systems
 - Existing building façade renovations
 - Masonry wall systems
 - Metal panel wall systems
 - Curtain wall systems
 - Rain screens wall systems



RESEARCH PROCESS | Identified Commonalities

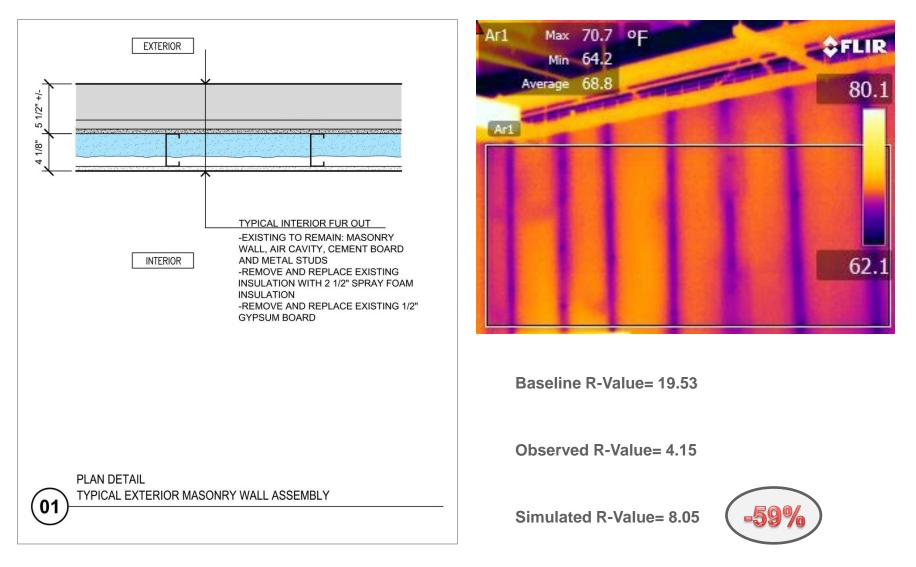
- Identified 16 common areas for further investigation
- Transitions and Penetrations
 - Transitions between new and existing facades
 - Transitions between different wall systems
 - Transition between windows and walls
 - Foundation to wall transitions
 - Roof to wall transitions
 - Roof parapets
 - Soffits
 - Roof penetrations
 - Seismic & movement joints
 - Louver openings



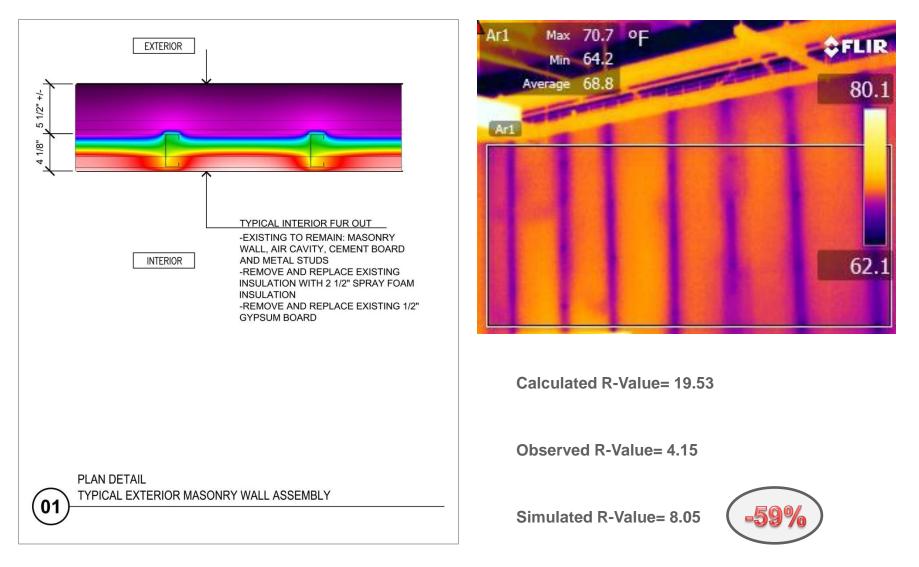




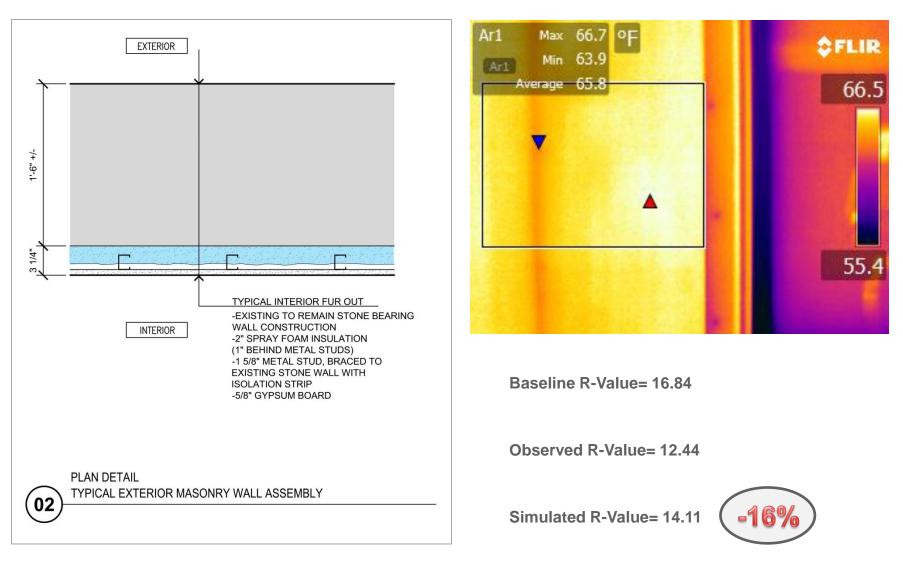
Building 1- studs directly attached to existing wall → resulting in a decrease of 59% of baseline R-value



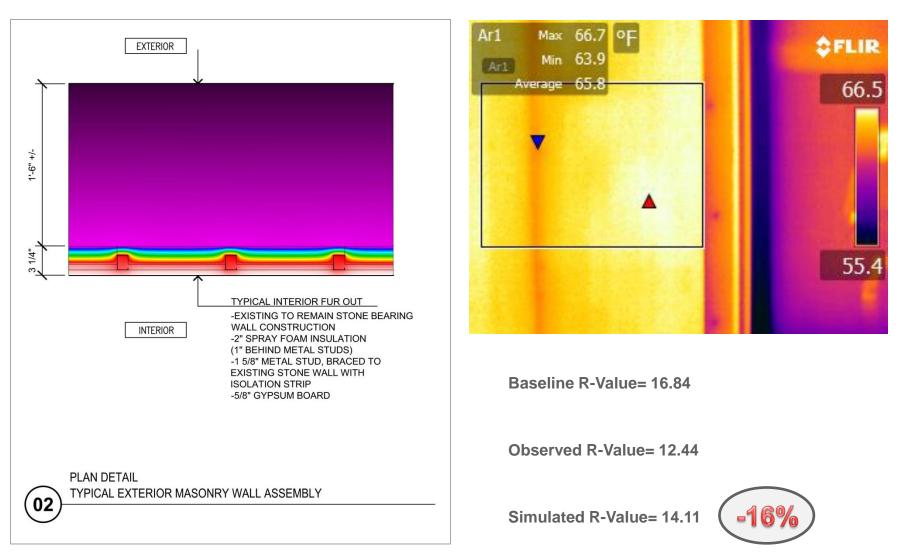
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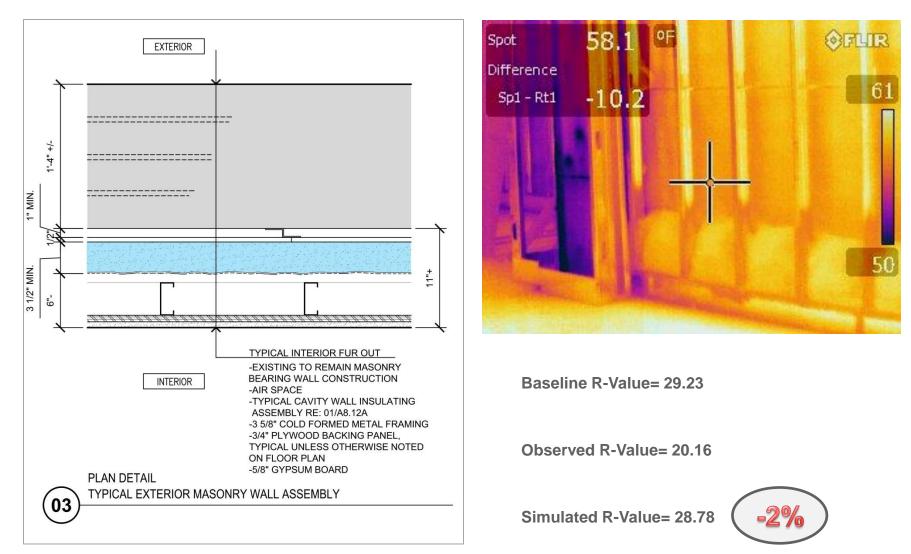
Building 2- studs pulled 1" back from existing wall \rightarrow results in a decrease of 16% of baseline R-value



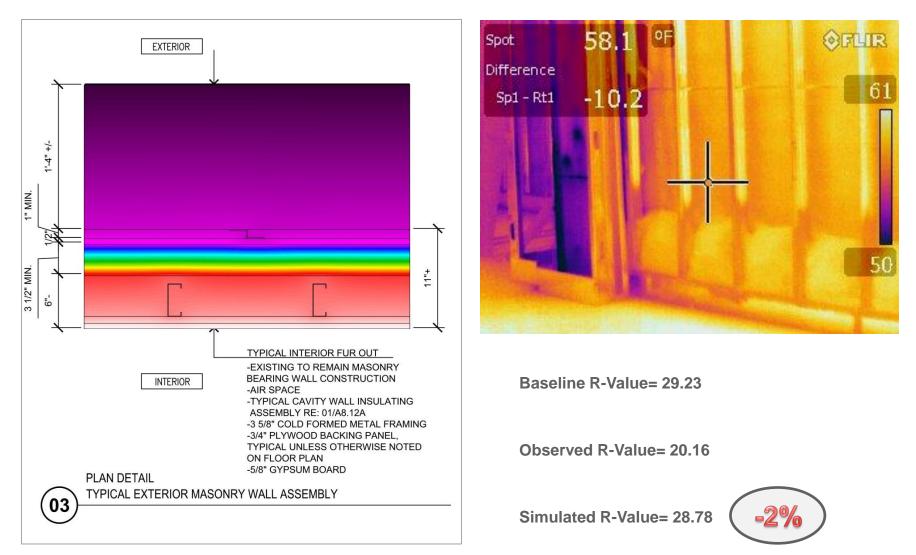
Building 2- studs pulled 1" back from existing wall \rightarrow results in a decrease of 16% of baseline R-value

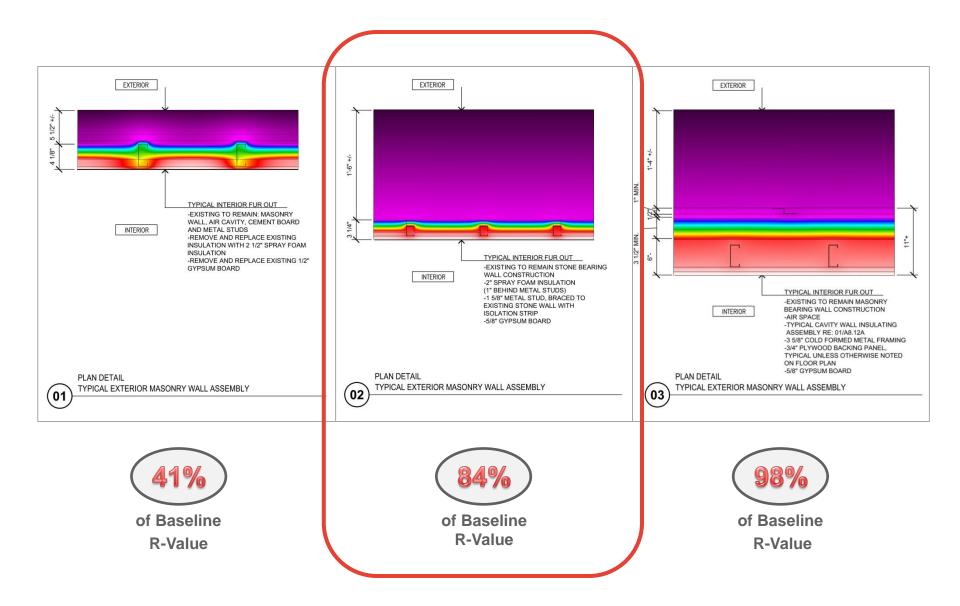


Building 3- studs separated from insulation → resulted in a decrease of 2% of baseline R-value

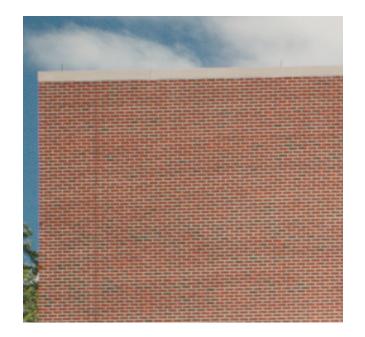


Building 3- studs separated from insulation → resulted in a decrease of 2% of baseline R-value

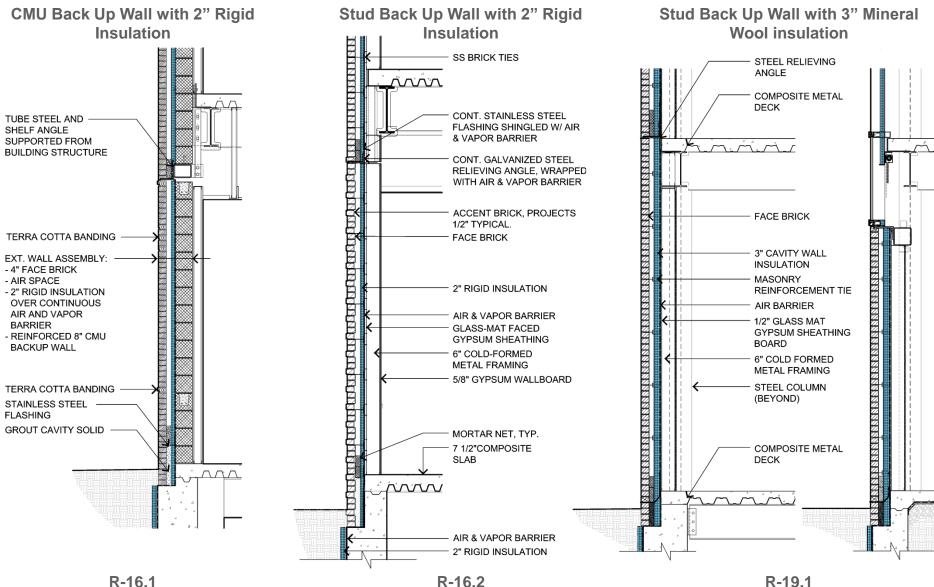








- Main areas of thermal bridging:
 - Brick ties (one every 2.67 square feet)
 - Shelf angle



R-16.1

CMU Back Up Wall with 2" Rigid Insulation Stud Back Up Wall with 2" Rigid Insulation Stud Back Up Wall with 3" Mineral Wool insulation











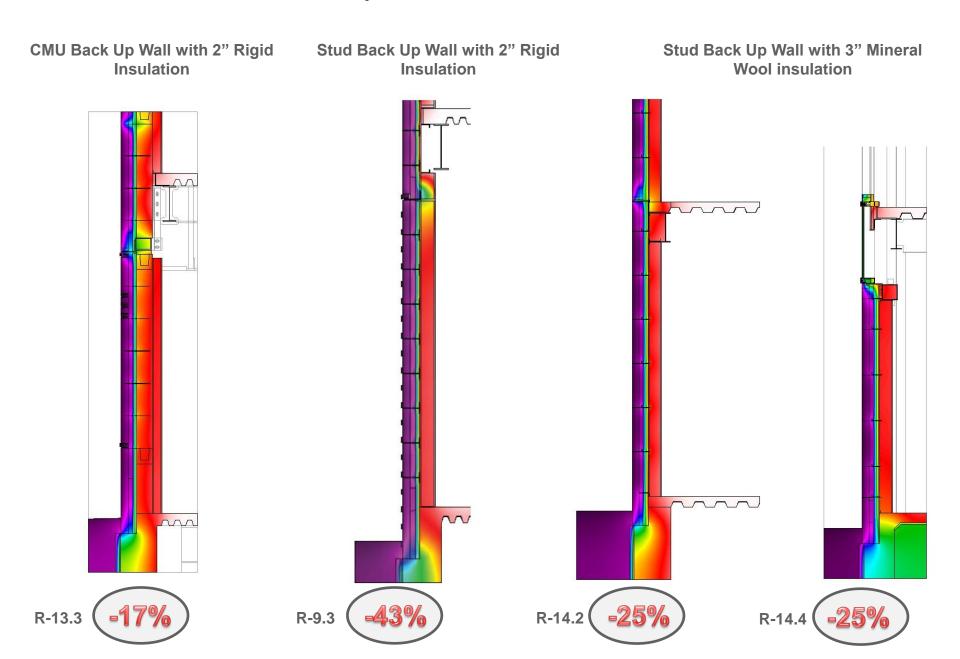






R-12.3

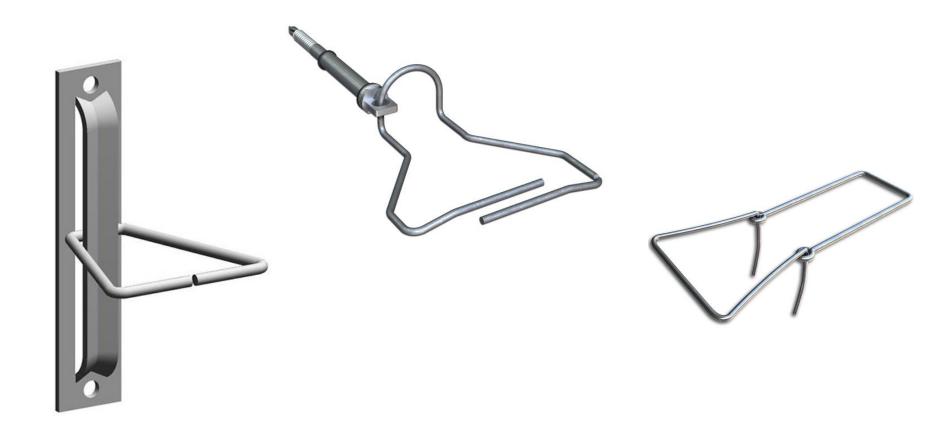




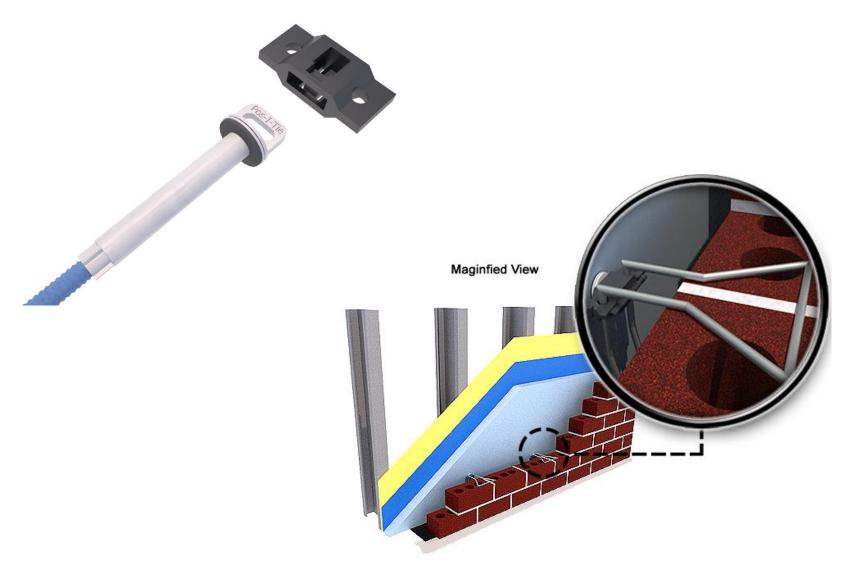
Screw On (S)

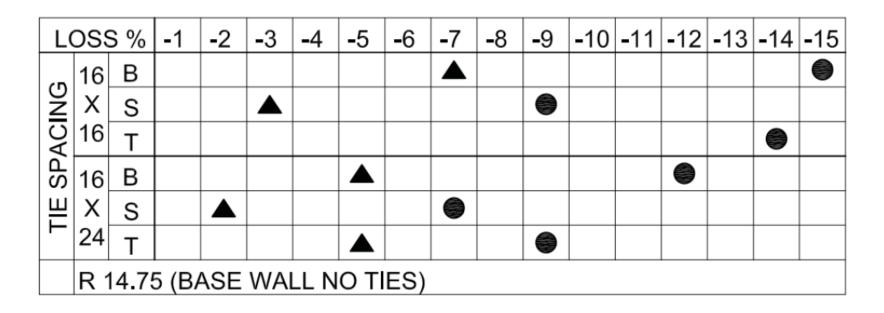
Posities Barrel (B)

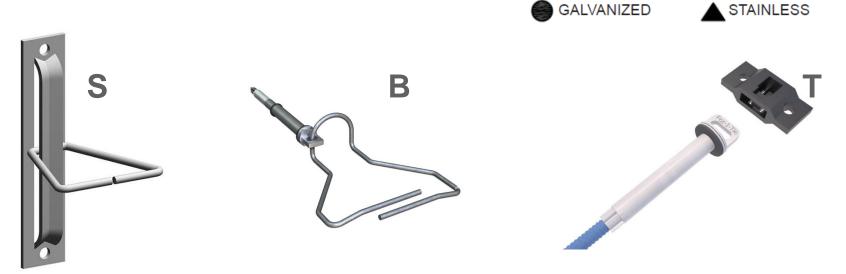
Eye and Pintle

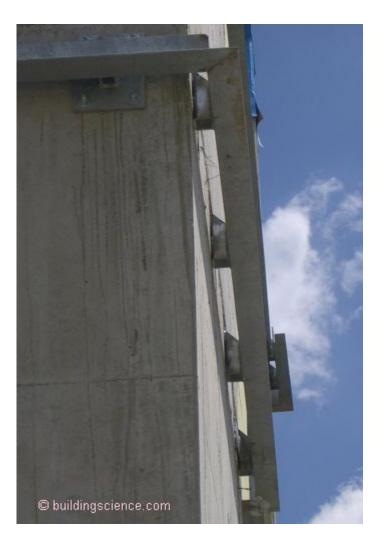


Thermal Brick Tie (T)

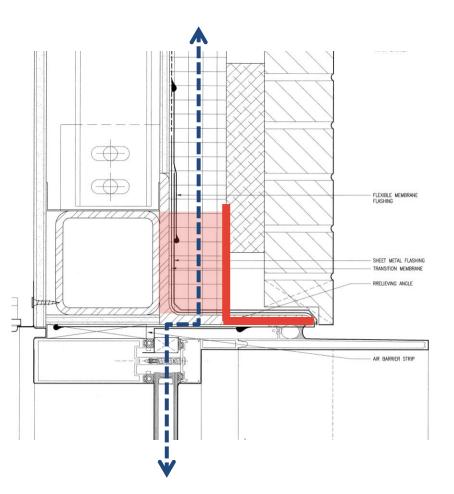


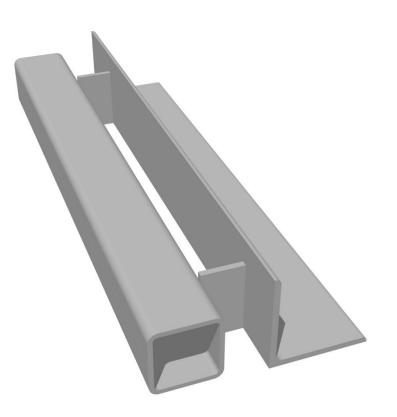


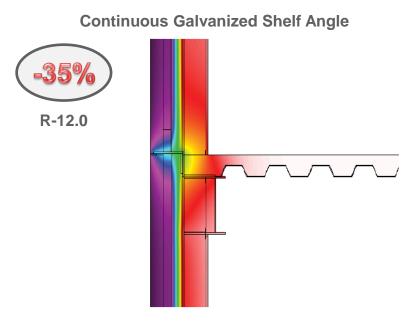




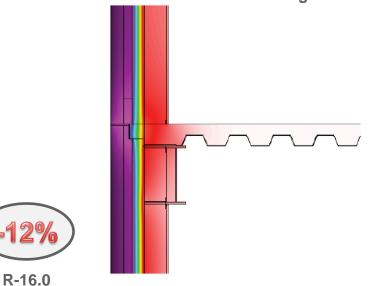


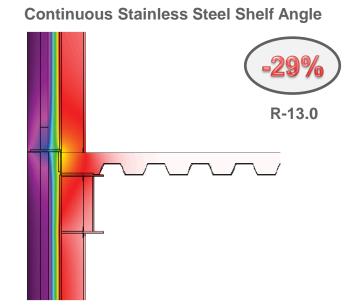




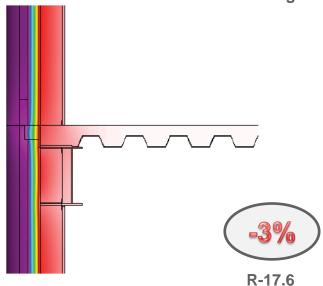


Discontinuous Galvanized Shelf Angle

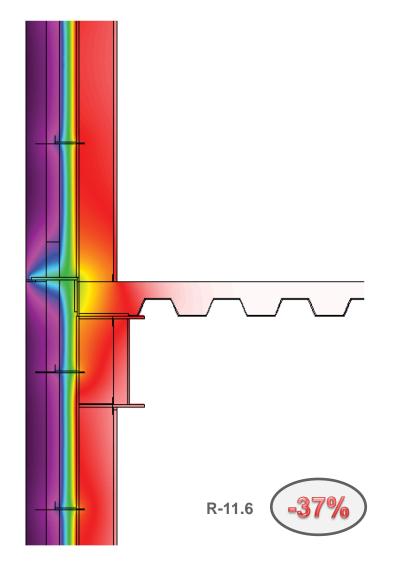




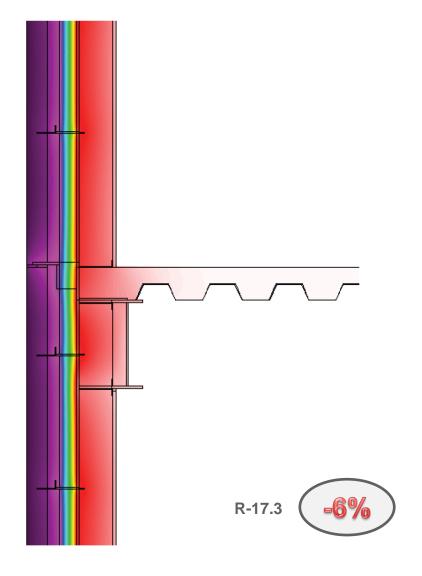
Discontinuous Stainless Steel Shelf Angle



Traditional Masonry Wall with Galvanized Barrel Ties and a Continuous Galvanized Shelf Angle



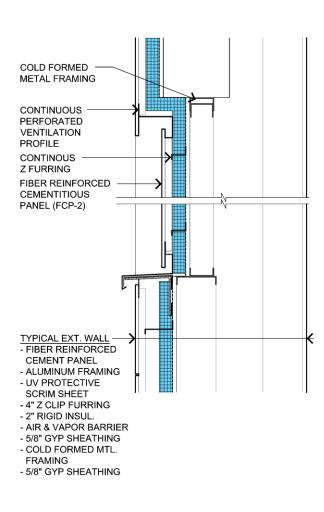
Improved Masonry Wall with Stainless Steel Screw Ties and a Discontinuous Stainless Steel Shelf Angle



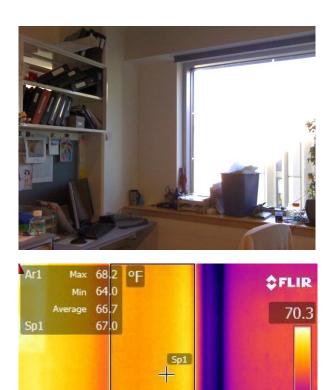


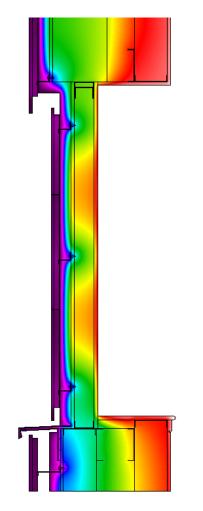


Horizontal Z-Girt Supports



R-14.1



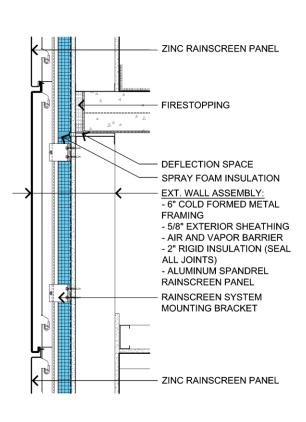


R-6.2

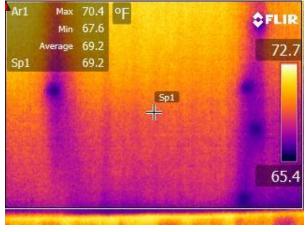




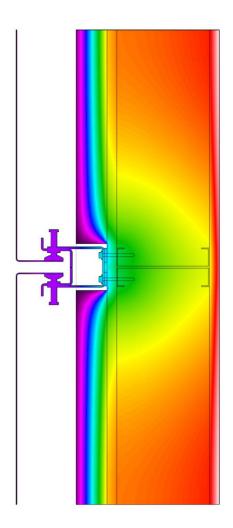
Clip Supports







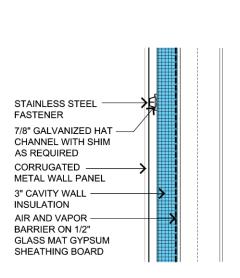
R-9.7



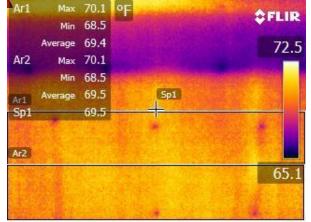


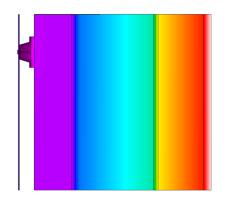


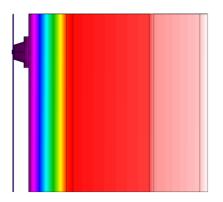
Vertical Z-Girt Supports









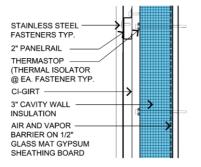


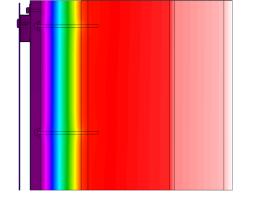




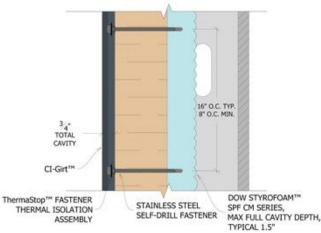


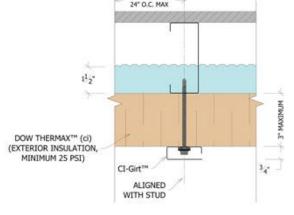




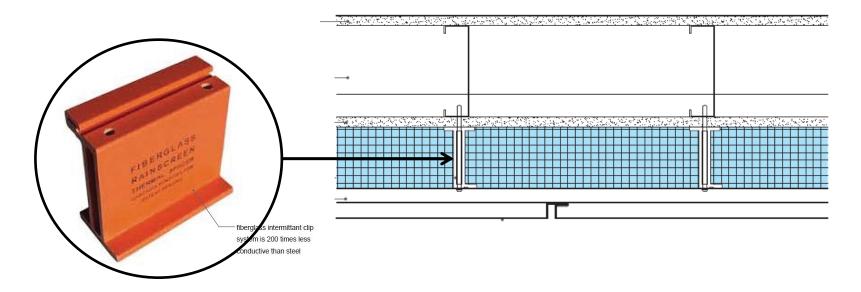


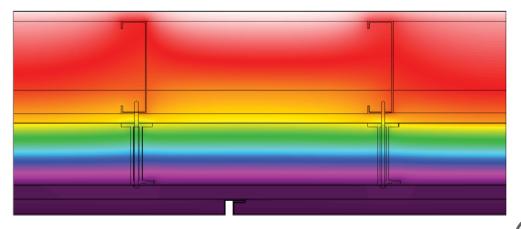






Examples of existing thermally broken products on the market

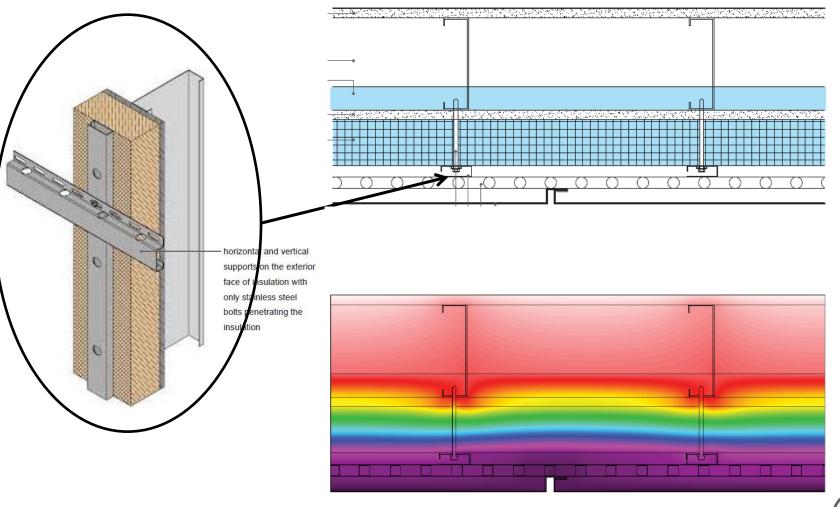








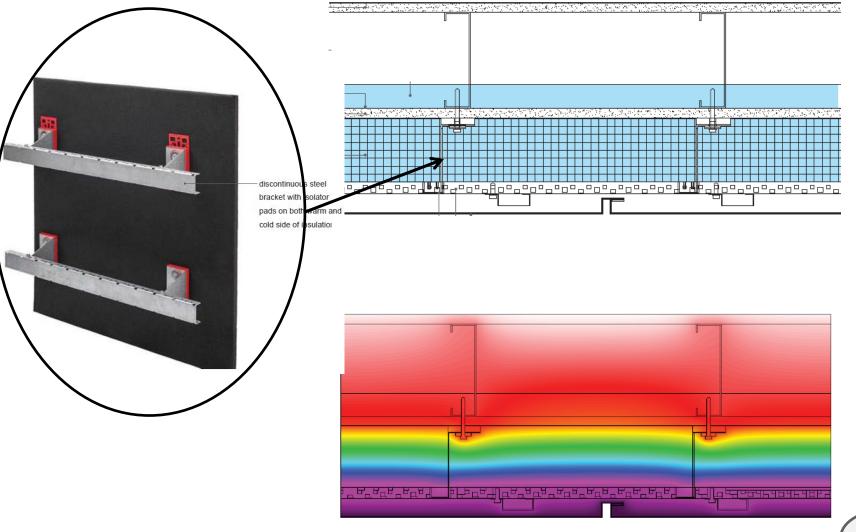
Examples of existing thermally broken products on the market



R-21.4



Examples of existing thermally broken products on the market



R-22.5

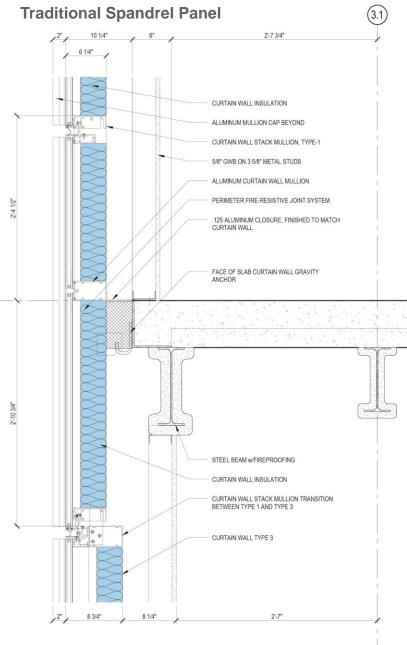


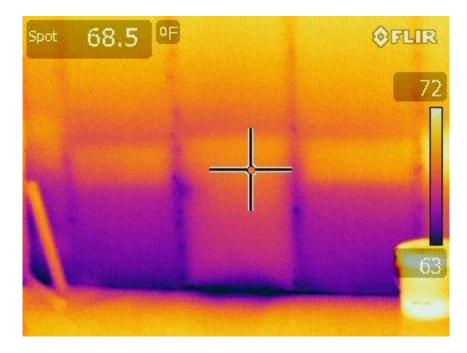
RESEARCH FINDINGS | Curtain Walls





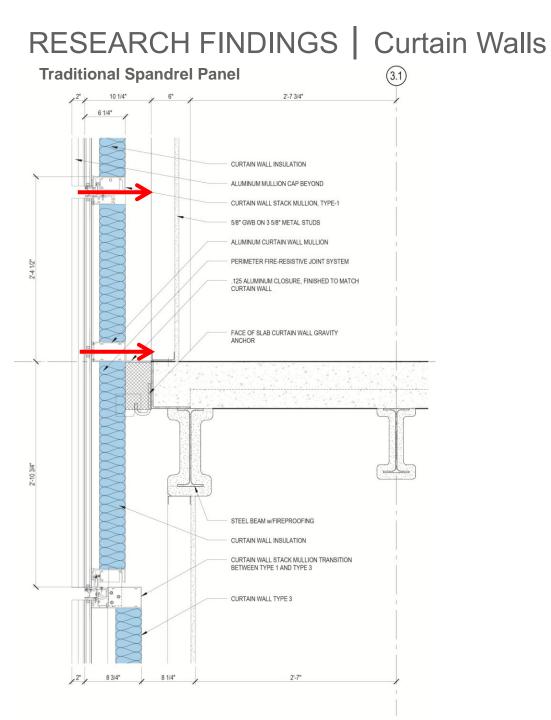
RESEARCH FINDINGS | Curtain Walls

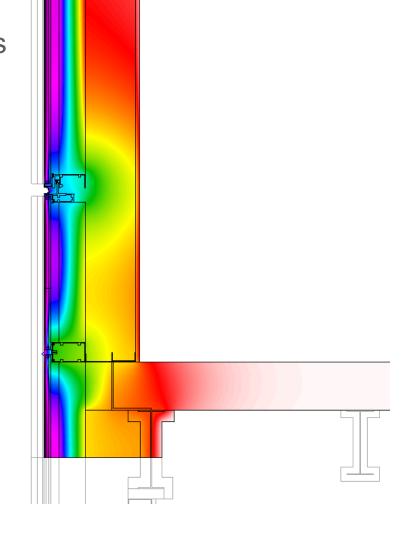






Baseline R-Value: 20.4 Observed R-Value: 5.8

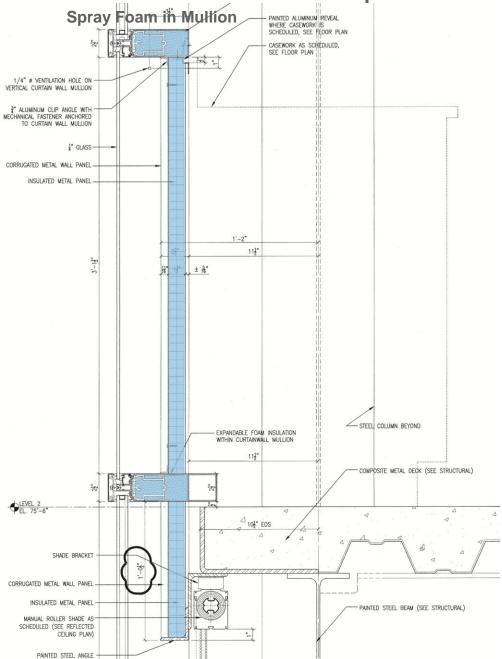


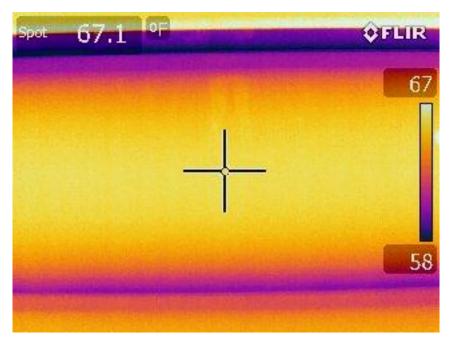




Baseline R-Value: 20.4 Simulated R-Value: 6.2

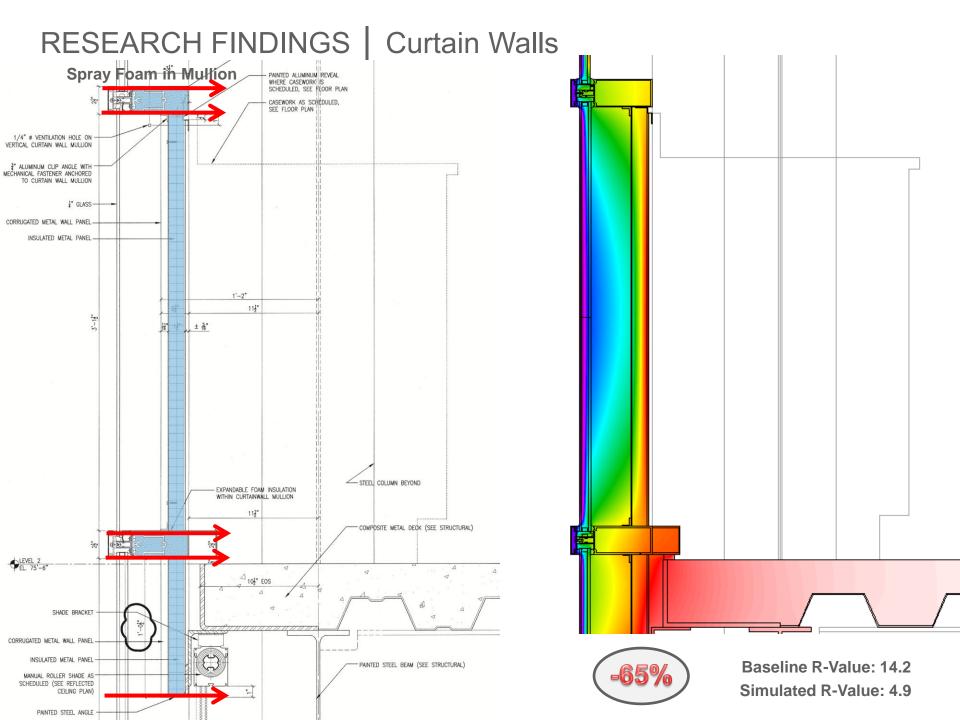
RESEARCH FINDINGS | Curtain Walls



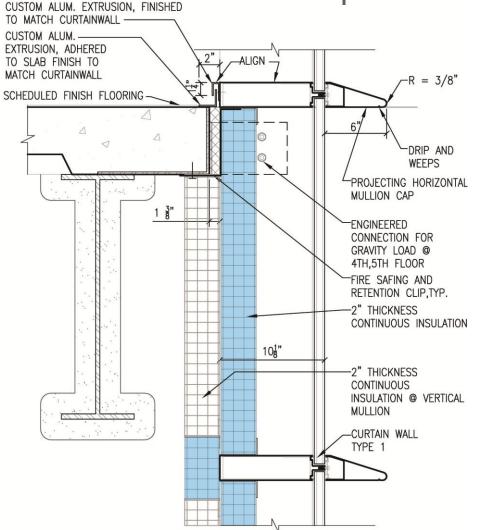




Baseline R-Value: 14.2 Observed R-Value: 6.2

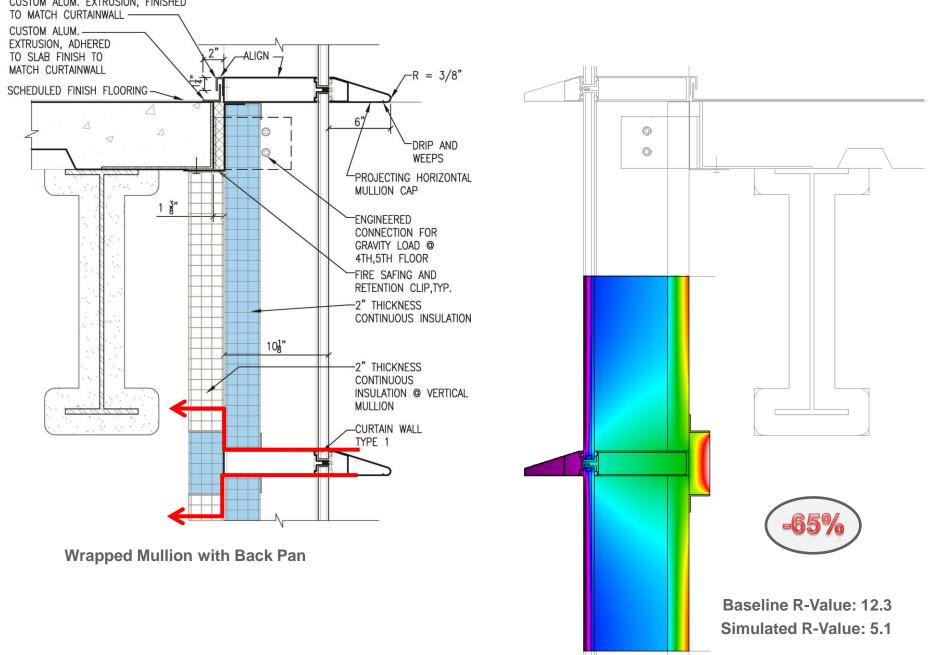


RESEARCH FINDINGS Curtain Walls

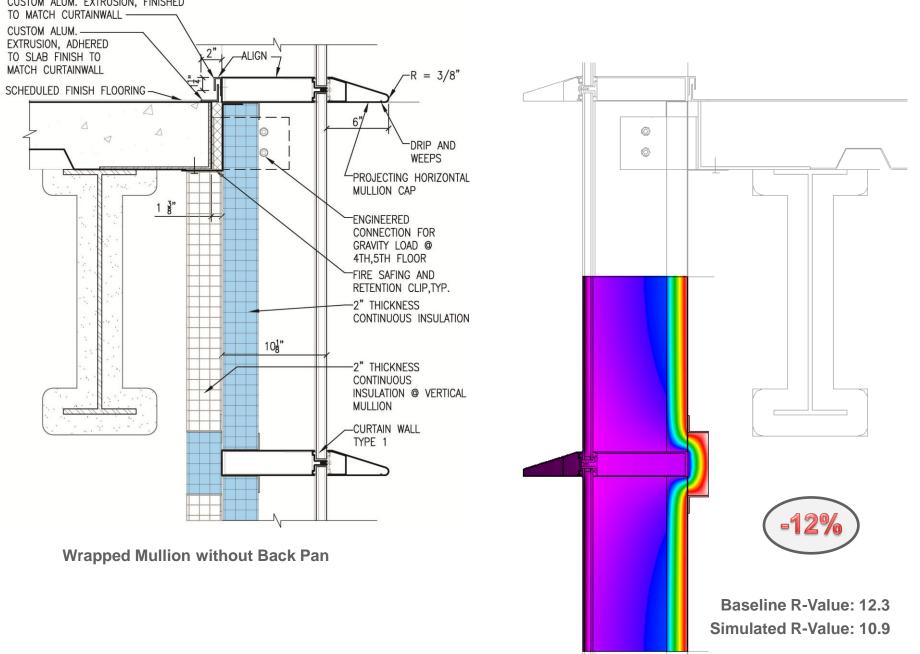


Wrapped Mullion

RESEARCH FINDINGS Curtain Walls

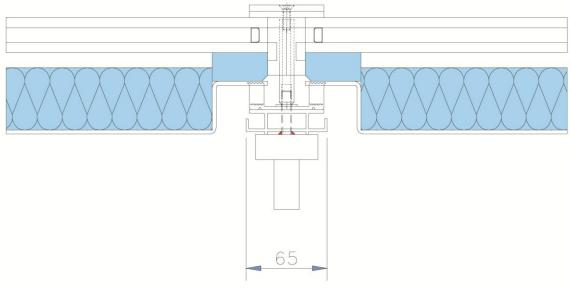


RESEARCH FINDINGS Curtain Walls



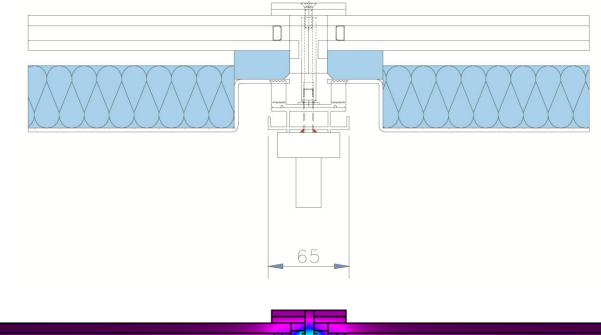
RESEARCH FINDINGS | Curtain Walls

Glazed in Spandrel Panel



RESEARCH FINDINGS | Curtain Walls

Glazed in Spandrel Panel

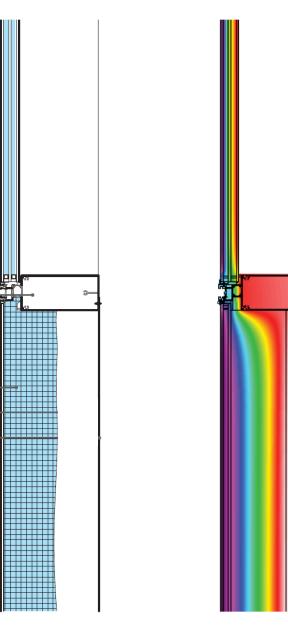




Baseline R-Value: 10.6 Simulated R-Value: 8.1

RESEARCH FINDINGS | Curtain Walls

Glazed in Spandrel Panel

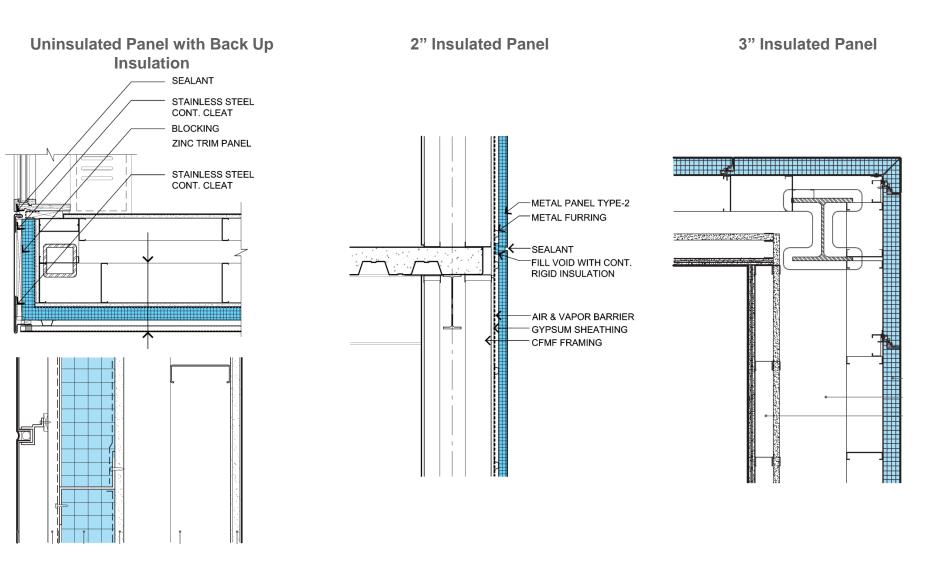




Baseline R-Value: 21.2 Simulated R-Value: 15.1



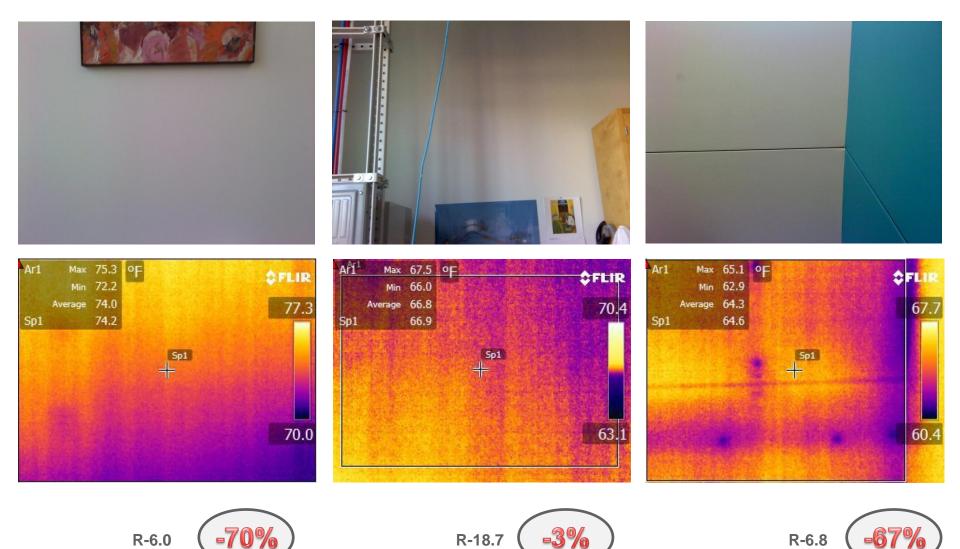




Uninsulated Panel with Back Up Insulation

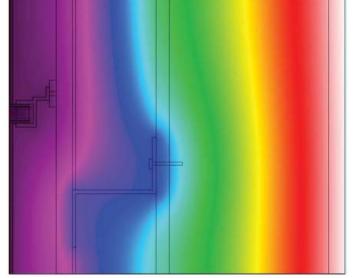
2" Insulated Panel

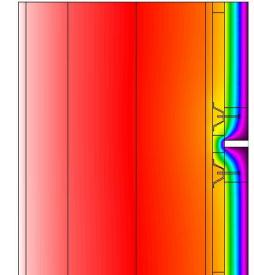
3" Insulated Panel

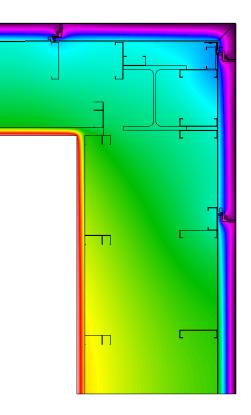


Uninsulated Panel with Back Up Insulation 2" Insulated Panel

3" Insulated Panel









R-17.6



RESEARCH FINDINGS | Window Openings



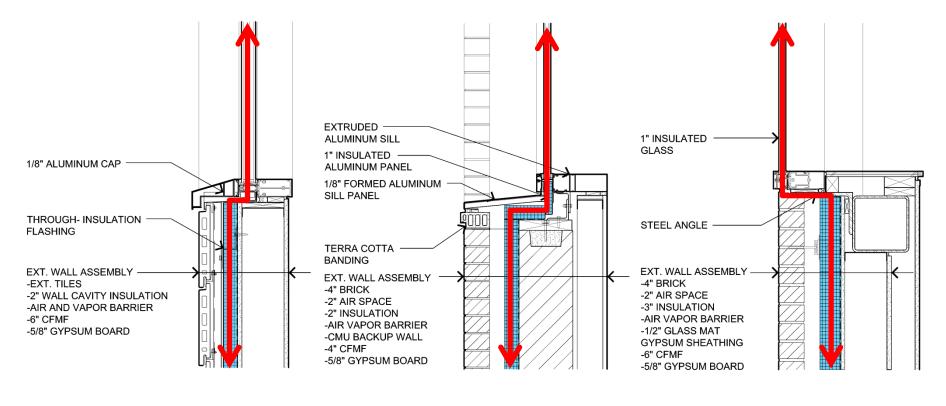




Inline

Recessed

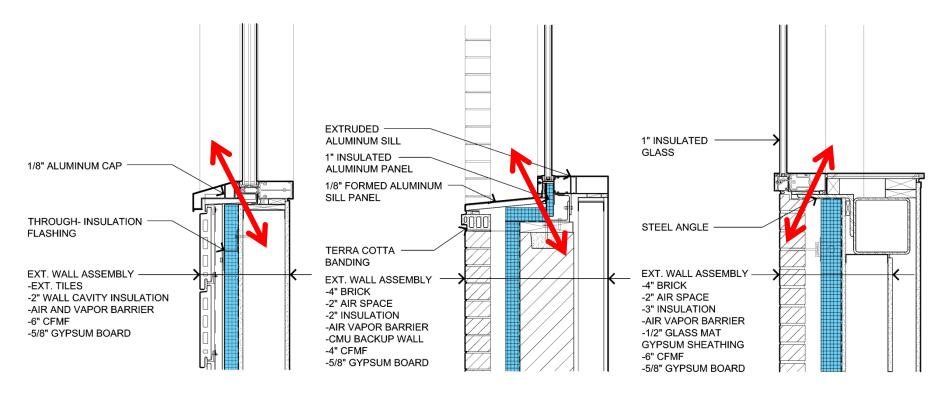
RESEARCH FINDINGS | Window Openings – Thermal Barrier



Aligned

Recessed

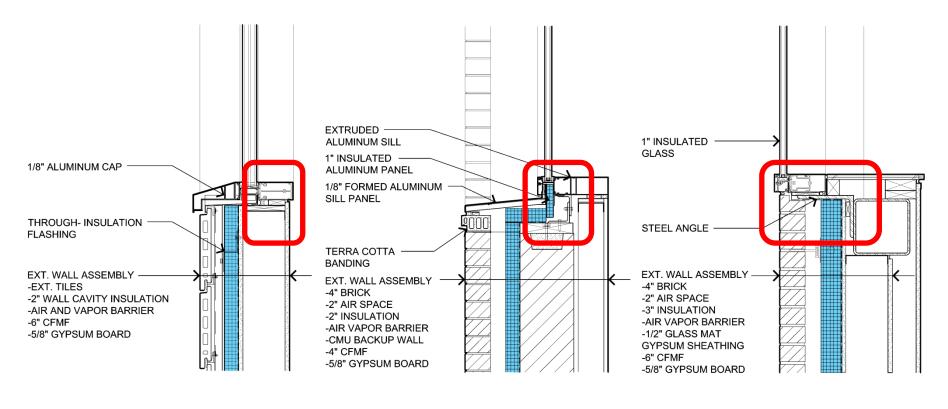
RESEARCH FINDINGS | Window Openings – Flanking Loss



Aligned

Recessed

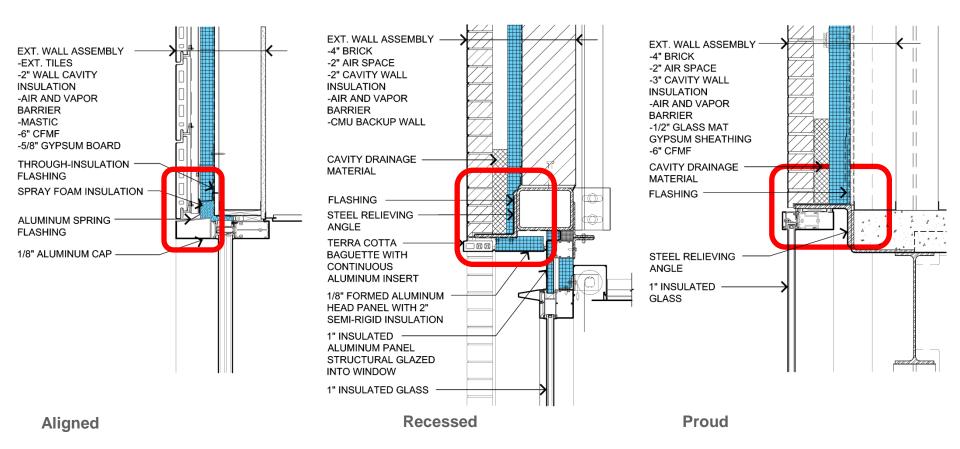
RESEARCH FINDINGS | Window Openings – Structural Support



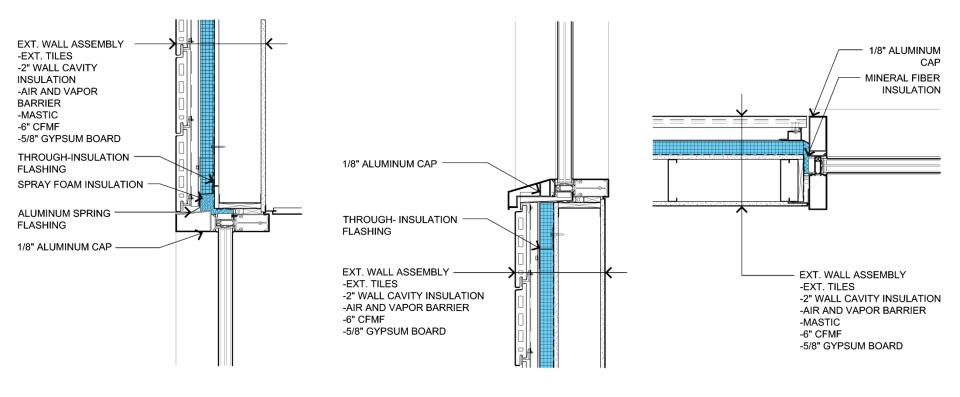
Aligned

Recessed

RESEARCH FINDINGS | Window Openings – Structural Support



RESEARCH FINDINGS | Window Openings – Inline Relationship



Window Head

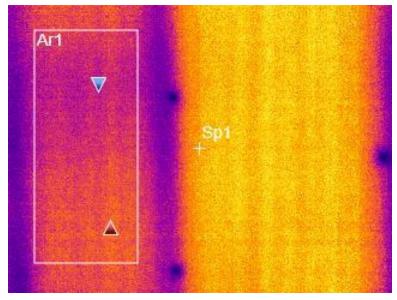
Window Sill

Window Jamb

RESEARCH FINDINGS | Window Openings – Inline Relationship



Window Jamb

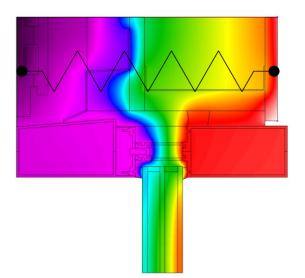


Window Jamb



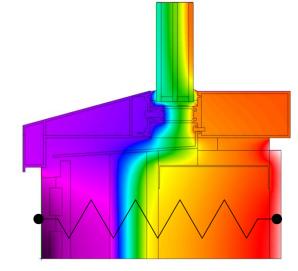
R-7.50

RESEARCH FINDINGS | Window Openings – Inline Relationship



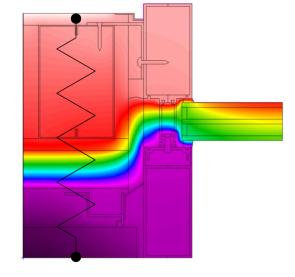
Window Head





Window Sill

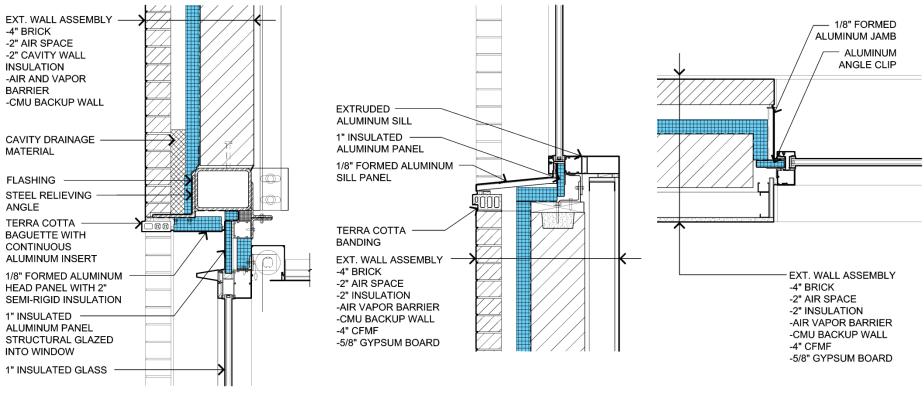




Window Jamb



RESEARCH FINDINGS | Window Openings – Recessed Relationship



Window Head

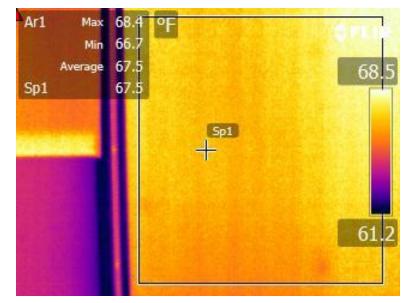
Window Sill

Window Jamb

RESEARCH FINDINGS | Window Openings – Recessed Relationship



Window Jamb

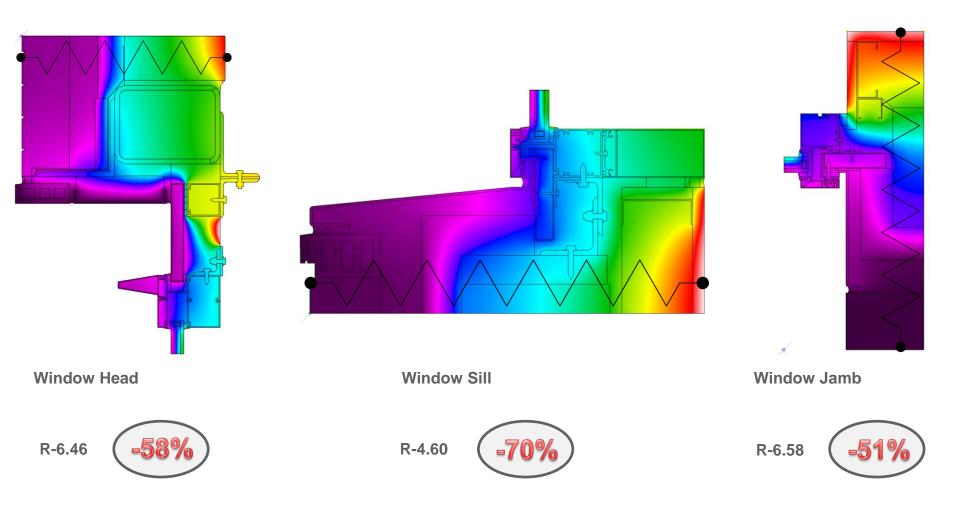




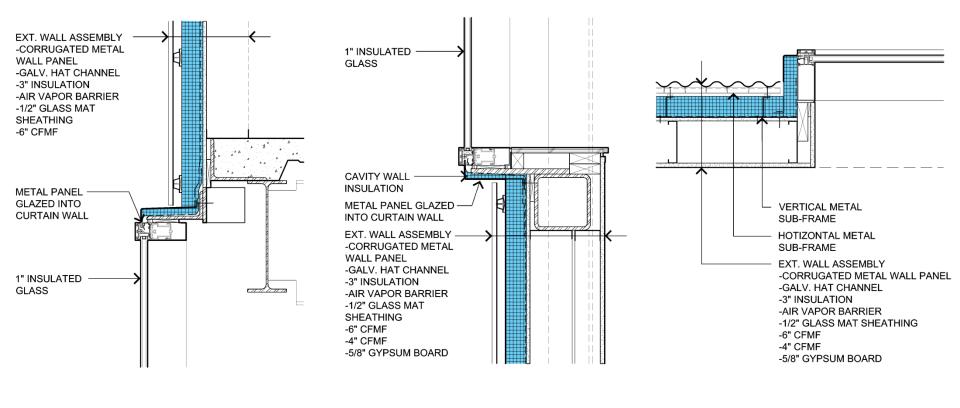


R-6.58

RESEARCH FINDINGS | Window Openings – Recessed Relationship



RESEARCH FINDINGS | Window Openings – Proud Relationship



Window Head

Window Sill

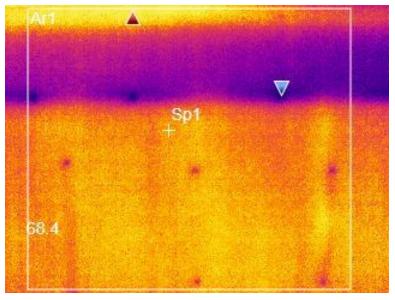
Window Jamb

Calculated Clear Wall R-Value: 18.78

RESEARCH FINDINGS | Window Openings – Proud Relationship



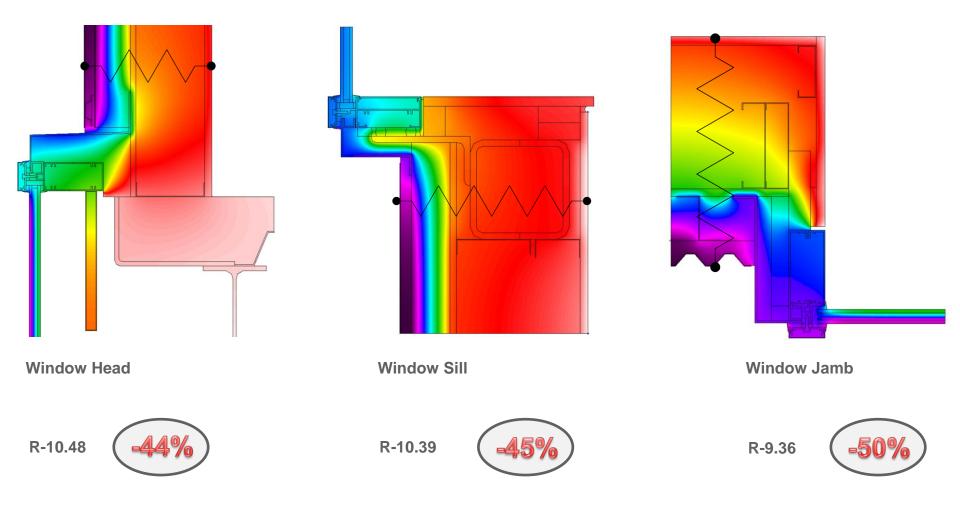
Window Sill



Window Sill



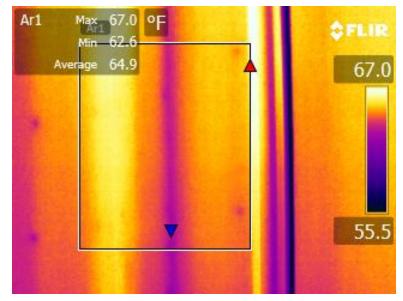
RESEARCH FINDINGS | Window Openings – Proud Relationship



RESEARCH FINDINGS | Window Openings – Aligned



Window Jamb





R-7.94

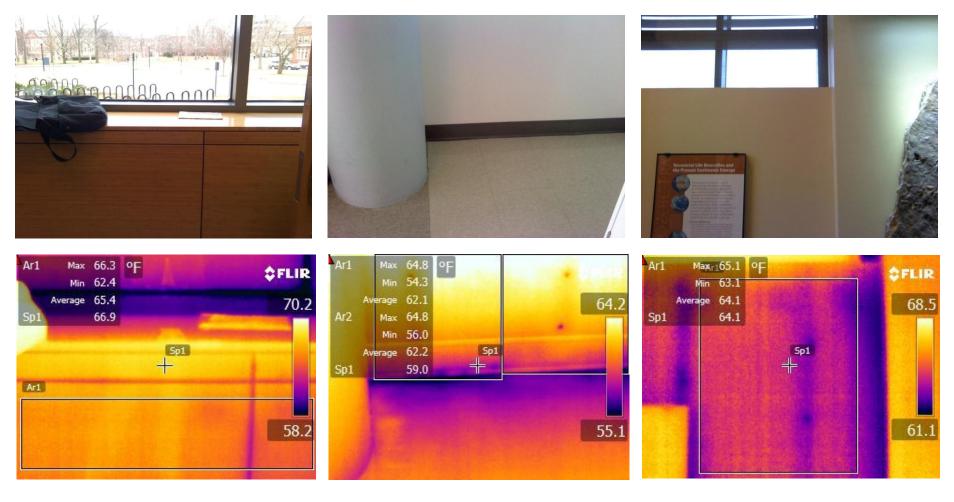




Exterior Insulation

Interior Insulation

Exterior Insulation

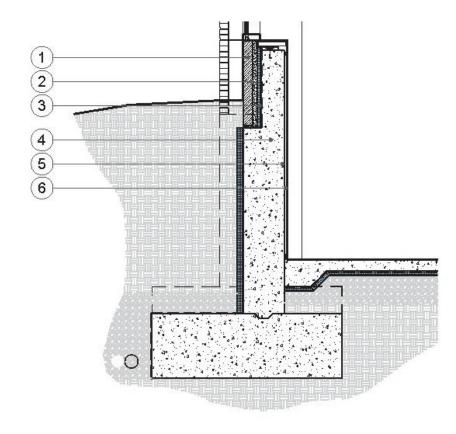


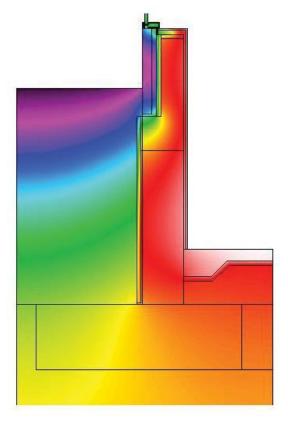




R-3.5

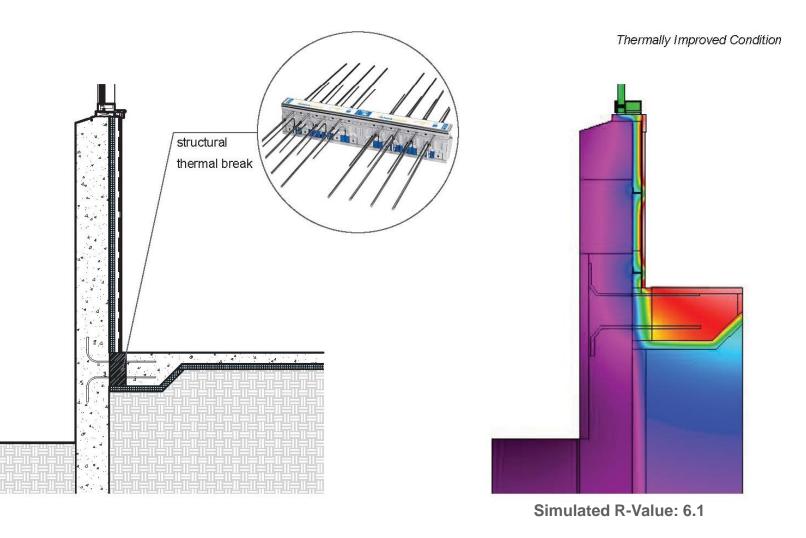
R-4.1





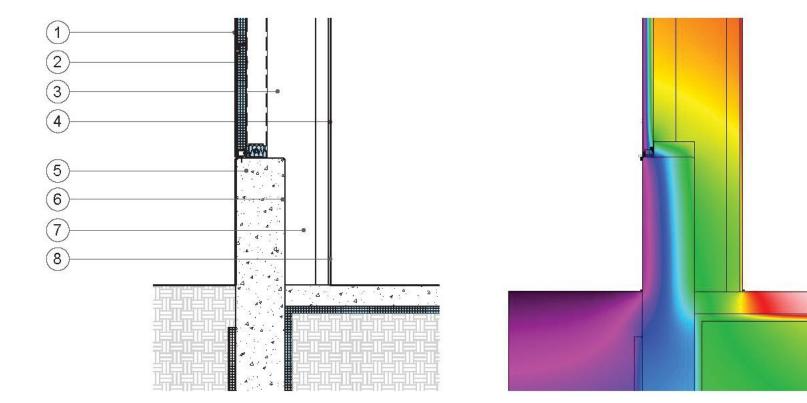
Simulated R-Value: 8.39





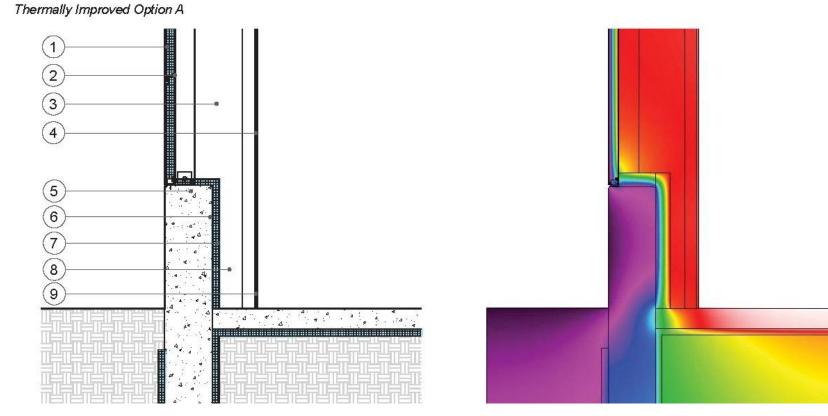


As-Built Condition



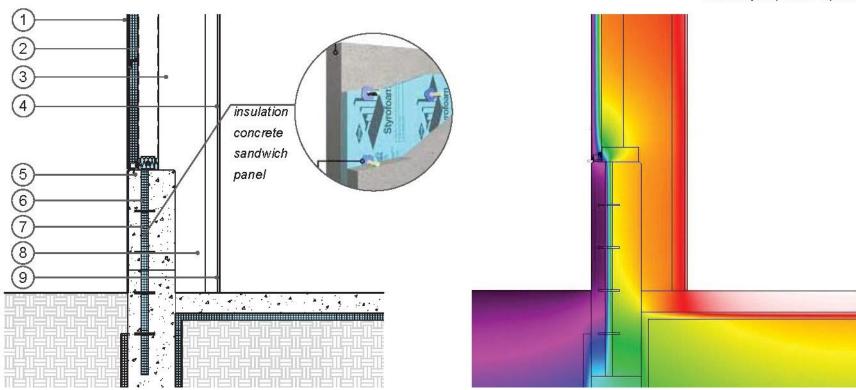
Simulated R-Value: 4.10

-69%



Simulated R-Value: 8.59





Thermally Improved Option B

Simulated R-Value: 9.82

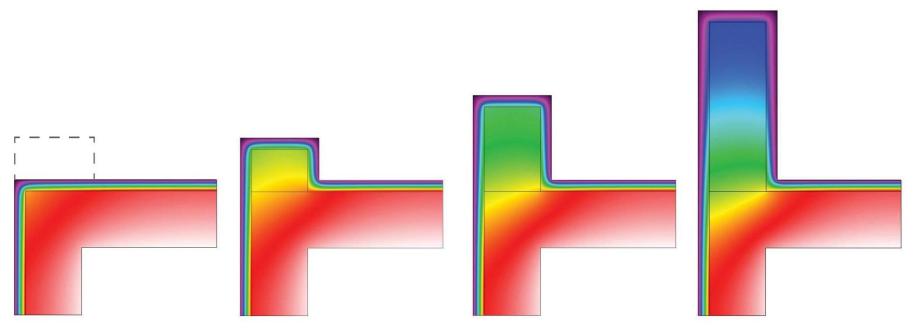


RESEARCH FINDINGS | Roof Parapets





RESEARCH FINDINGS | Parapets



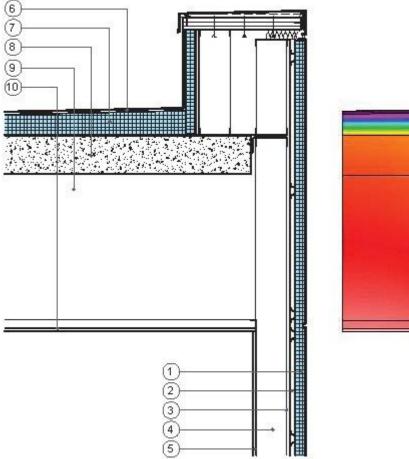
R-15.33 Insulating beneath parapet

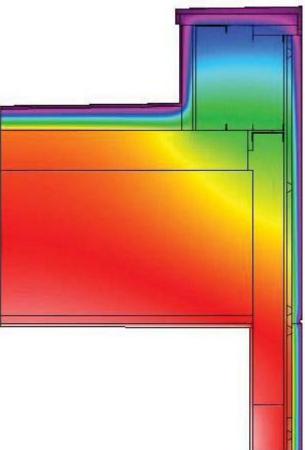
R-13.42 Insulating around 1'-3" tall parapet R-12.25 Insulating around 2'-6" tall parapet R-11.27 Insulating around 5'-0" tall parapet

as the height increases, the R-value decreases

RESEARCH FINDINGS | Parapets

As-Built Condition



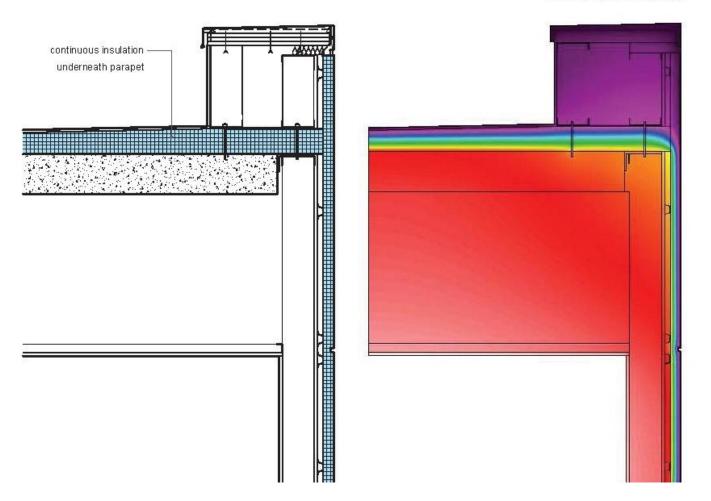


Simulated R-Value: 8.57



RESEARCH FINDINGS | Parapets

Thermally Improved Condition



Simulated R-Value: 10.65



CONCLUSION | Full Report

 Report available on Payette's website

> Projects Research @ Payette Thermal Performance of Façades



Final Report | May 2014



CONCLUSION | Observations

- Thermal bridges are significantly decreasing the thermal performance of our building envelopes
- There are numerous thermal bridges all over our buildings
- Careful detailing and attention to the issue can improve their performance
- More awareness and education is needed on the sources of thermal bridges in our details
- We should shift the dialog from the R-value of insulation to the performance as R-value of assembly
- **CONTINUITY** of insulation barrier key to good thermal performance



Questions?

INTERACTIVE WORKSHOP | Finding Solutions to Thermal Bridges

- Break into Groups (20 Minutes)
 - Review your typical building envelope detail
 - Identify the thermal break(s)
 - Develop your own solution(s)
- Share you Findings and Proposed Solutions (10 Minutes)

- 1) Transitions Between Systems
- 2) Soffits
- 3) Roof to Wall Transitions

- 4) Roof Penetrations / Seismic Joints
- 5) Louvers
- 6) Exist. Bldg. Slab & Beam Conx.